APPENDIX A

Reprints of OH Rate Constant Determination $\qquad \text{and Reactivity Scale Papers}$

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Relative Rate Constants for Reaction of the Hydroxyl Radical with a Series of Alkanes, Alkenes, and Aromatic Hydrocarbons

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The relative rates of disappearance in air at 305 \pm 2 K of a set of 14 alkanes, alkenes, and aromatic hydrocarbons were measured in an environmental chamber under simulated atmospheric conditions. The observed rates of disappearance were used to derive relative rates of reaction with the hydroxyl radical (OH) on the previously validated basis that OH is the species dominantly responsible for the hydrocarbon disappearance under the experimental conditions employed. Absolute rate constants, obtained from the relative values by using the mean of the published rate constants for OH + n-butane (1.8 × 10⁹ M⁻¹ s⁻¹), are ($k \times 10^{-9}$ M⁻¹ s⁻¹): isopentane, 2.0 \pm 0.4; 2-methylpentane, 3.2 \pm 0.6; 3-methylpentane, 4.3 \pm 0.9; n-hexane, 3.8 \pm 0.8; m-xylene, 12.9 \pm 2.6; n-propylbenzene, 3.7 \pm 0.8; isopropylbenzene, 3.7 \pm 0.8; ethylbenzene, 4.8 \pm 1.0; o-ethyltoluene, 8.2 \pm 1.6; m-ethyltoluene, 11.7 \pm 2.3; p-ethyltoluene, 7.8 \pm 1.6; ethene, 5.2 \pm 1.0; propene, 17.5 \pm 3.5; cis-2-butene; 39.2 \pm 8.0; 1,3-butadiene, 46.4 \pm 9.3. In the case of seven of the compounds investigated these results are shown to be in good agreement with literature values reported for elementary rate constant determinations. For the remaining seven compounds no previous determinations have been made.

Introduction

The hydroxyl radical is well known to be an important species in the chemistry of combustion systems, 1,2 the stratosphere, 3-5 and the troposphere. 6-9 Recent direct determinations of its concentration in ambient air 10,11 have

shown average daytime levels of about 5 \times 10⁶ molecule cm⁻³ in good agreement with predictions from computer models of the formation of photochemical air pollution.^{6,12–14}

In order to develop satisfactory chemical mechanisms for modeling combustion and photooxidation systems including urban airshed models, 15,16 kinetic data for the reactions of the OH radical with hydrocarbons, as well as various inorganic species, are necessary. Prior to 1970 relatively few absolute rate constants were available for OH reactions with organic species; however, since then a large number of determinations have been reported for alkanes¹⁷⁻²⁷ and alkenes. 21-23,28-36 Although aromatic compounds such as toluene, xylenes, propylbenzene, m-ethyltoluene, and 1,2,3and 1.2.4-trimethylbenzenes are present in polluted ambient air,37-39 only in the past few years have significant studies been reported on the reactions of the OH radical with some of these aromatics. 21,40-42 For example, recently we reported the use of an environmental chamber to obtain accurate relative rate constants for the gas phase reaction of hydroxyl radicals with a series of aromatic hydrocarbons using n-butane as the reference compound.42 Although a number of other species are present in these experiments (i.e., O(3P), HO2, O3, NO3, etc.), with the exception of O3 in the case of the alkenes, these species have been shown to make at most minor contributions to the observed disappearance of the hydrocarbons investigated. Thus, the rate constants determined in our previous study42 are in good agreement with those determined subsequently in separate studies of the reactions of individual compounds with OH using a flash photolysis-resonance fluorescence technique.^{40,41}

On the basis of this validation of the environmental chamber method, we have extended our investigation to include an additional six aromatic hydrocarbons, four alkanes, and four alkenes.

Experimental Section

Irradiations of the HC-NO_x-air system were carried out in an all-glass (Pyrex) chamber of approximately 6400-l. volume equipped with two externally mounted, diametrically opposed banks of Sylvania 40 BL fluorescent lamps. 43 Before each experiment the chamber was flushed for a minimum of 2 h at a rate of 12–15 scfm with a purified air stream. 44 The resulting matrix air contained less than \sim 1 × 10^{-9} M (100 ppb C) of nonmethane hydrocarbons. All reactants were injected into the chamber using 100-ml precision bore syringes and rapid mixing was obtained using Teflon-coated sonic pumps. During irradiation, the chamber temperature was maintained at 305 \pm 2 K by passing chilled air between the chamber walls and the fluorescent lamp banks.

Hydrocarbon disappearance was measured by gas chromatography using the columns and techniques developed by Stephens and Burleson.^{37,45} Ozone⁴⁶ was monitored by means of ultraviolet absorption (Dasibi Model 1003 analyzer), carbon monoxide by gas chromatography (Beckman 6800 Air Quality analyzer), and NO-NO₂-NO_x by the chemiluminescent reaction of NO with ozone (TECO Model 14B).

The concentrations of the reactants ranged between 4.5 and 9.0×10^{-10} M (11–22 ppb in air) except for ethene, ethane, acetylene, and n-butane whose concentrations were 1.8, 3.7, 1.8, and 8.3×10^{-9} M (45, 92, 45, and 203 ppb in air), respectively. In addition low concentrations of carbonyl compounds (formaldehyde, acetaldehyde, and acetone) were present. Initial concentrations in the photolysis experiments were 27×10^{-9} M (2900 ppb C) of total nonmethane hydrocarbons, 1.75×10^{-9} M (0.43 ppm) of NO_x (with an NO₂/NO_x ratio of 0.12), 28.5×10^{-9} M (7 ppm) of CO, and 112.9×10^{-9} M (2775 ppb) of methane together

with water at 50% relative humidity. Four replicate experiments were carried out in which this mixture was irradiated for 3 h with continuous analysis of inorganic species and analysis of hydrocarbons every hour. The irradiation period was extended from 2 to 3 h compared with our earlier study in order to obtain additional data points. The light intensity, measured as the rate of NO2 photolysis in nitrogen, k₁,⁴⁷ was approximately 0.26 min⁻¹. All data were corrected for losses due to sampling from the chamber (0.9-2.0%/h) by subtraction of the average dilution rate from the observed hydrocarbon disappearance rate. Although the HC/NO_x ratio was chosen to delay the formation of ozone, after 3 h of irradiation the ozone concentration was 0.065×10^{-9} M (0.016 ppm) or less in three of the runs and 0.13×10^{-9} M (0.031 ppm) in the fourth (which had a higher initial formaldehyde concentration). A small correction for loss of hydrocarbon due to reaction with ozone was applied to the alkene disappearance rates.

Results

The rates of disappearance observed during a 3-h run for the seven aromatic hydrocarbons, four alkanes, and four alkenes are shown in Figures 1-3, respectively (n-butane is included as the reference compound in each figure). Table I gives the disappearance rates for these reactants (after application of the dilution correction and for alkenes, the ozone correction), relative to that for n-butane, based on data from the four separate experiments.

With the assumption that the OH radical is the species responsible for the hydrocarbon depletion during the 3-h irradiation, absolute rate constants were derived from the relative rates of disappearance using a value of 1.8×10^9 M⁻¹ s⁻¹ as the mean of the existing literature values for the reaction of OH with n-butane^{21,23,24,27}

$$OH + n - C_4H_{10} \rightarrow H_2O + C_4H_9$$
 (1)

These results are shown in Table I and are compared with existing literature values whenever possible in Table II.

Discussion

As seen from Table II, the validation of the assumption that the OH radical is by far the major species depleting the hydrocarbons (during the first 2-3 h of reaction) has been provided by the good agreement observed between OH rate constants determined in our previous chamber study⁴² for benzene, toluene, o-, m-, and p-xylenes, and the trimethylbenzenes with those determined in elementary reaction studies of each individual hydrocarbon. 40,41 The extent to which this assumption is valid is indicated by the results of computer modeling calculations⁴⁸ (shown in Figure 4) for an HC-NO_x system of overall concentrations identical with that used in this study. In the computer simulation a propene and n-butane mixture was used as a surrogate for the complex hydrocarbon mixture employed in the experiment and the rate of attack on propene by OH, O₃, O(³P), and HO₂ was calculated. The relative and total concentrations of propene and n-butane were chosen such that the overall hydrocarbon reactivity toward the OH radical would equal that predicted for the complex mixture. It is clear from Figure 4 that, although OH is the major attacking species in these experiments, the O₃ contribution to the disappearance rates of the alkenes increases with time of irradiation. In contrast the rates of reaction of O₃ with alkanes and aromatics are many orders of magnitude slower⁵⁰⁻⁵² than with alkenes^{49,53} and no correction for

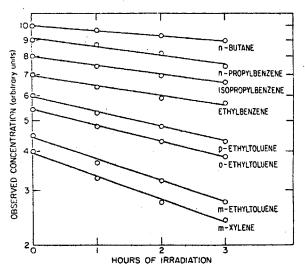


Figure 1. Logarithm of the aromatic hydrocarbon concentration during 3-h photolysis of HC-NO $_{\rm x}$ mixture in air at 305 \pm 2 K and 1 atm.

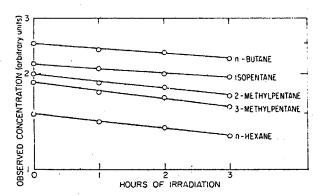


Figure 2. Logarithm of concentrations of alkanes during 3-h photolysis of HC-NO $_x$ mixture in air at 305 \pm 2 K and 1 atm.

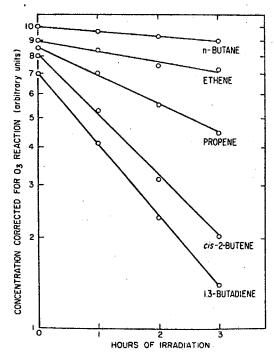


Figure 3. Logarithm of concentrations of alkenes during 3-h photolysis of HC-NO $_x$ mixture in air at 305 \pm 2 K and 1 atm.

TABLE I: Rates of Disappearance and Rate Constants for Selected Alkanes, Alkenes, and Aromatic Hydrocarbons at 1 atm in Air at 305 \pm 2 K

Compound	Relative rate of disappearance	10 ⁻⁹ k,° M ⁻¹ s ⁻¹
n-Butane	1	1.86
Isopentane	1.10	2.0 ± 0.4
2-Methylpentane	1.77	3.2 ± 0.6
3-Methylpentane	2.40	4.3 ± 0.9
n-Hexane	2.09	3.8 ± 0.8
m-Xylene	7.18	12.9 ± 2.6
n-Aylene n-Propylbenzene	2.07	3.7 ± 0.8
Isopropylbenzene	2.03	3.7 ± 0.8
Ethylbenzene	2.65	4.8 ± 1.0
o-Ethyltoluene	4.57	8.2 ± 1.6
m-Ethyltoluene	6.49	11.7 ± 2.3
p-Ethyltoluene	4.33	7.8 ± 1.6
	2.88	5.2 ± 1.0
Ethene	9.70	17.5 ± 3.5
Propene	25.8	46.4 ± 9.3
1,3-Butadiene cis-2-Butene	21.8	39.2 ± 8.0

^a The indicated error limits are ±20% and are the estimated overall error limits. ^b Placed on an absolute basis using the mean of the literature values; ref 21, 23, 24, and 27.

TABLE II: Rate Constants, k, for OH Radical Reactions with n-Butane and Selected Alkane, Alkenes, and Aromatic Hydrocarbons at Room Temperature

10-5	9k, M ⁻¹ s ⁻¹
Environmental d chamber studies ^{a,b}	Lit. values
≤2.3°	0.74 ± 0.07°
	0.95 ± 0.07^d
2.5 ± 0.9^a	3.47 ± 0.35^{c}
	3.67 ± 0.24^d
7.7 ± 2.3^{a}	9.18 ± 0.90 , c 11^{e}
14 ± 1^a	$14.2 \pm 1.4^{\circ}$
12.9 ± 2.6^{b}	11e
7.4 ± 1.5^a	7.32 ± 0.72,° 11°
th- 14 ± 3^a	15.8 ± 1.6°
:	
th- 20 ± 3^a	$20.1 \pm 2.0^{\circ}$
•	
th- 31 ± 4^a	$28.3 \pm 2.9^{\circ}$
•	
	2.7 ^f
$nt-$ 3.2 \pm 0.6 ^b	3.4 ^f
$nt-4.3 \pm 0.9^{b}$	3.4
3.8 ± 0.8^{b}	2.9f
5.2 ± 1.0^{b}	5.7 ± 0.6^{g}
	$1.1,^h 3.0,^i 3.2 \pm 0.4,^j$
	$3.0,^k$ 1.8 ± 0.6^l
	1.0 ± 0.3 , $m \cdot 1.3 \pm 0.1$ $n \cdot 1.3 \pm 0.1$
17.5 ± 3.5^{b}	21.7 ± 2.4^{g}
	10.2 ± 2.6^{h}
	8.7 ± 1.3 , l 15.1 ± 1.5 , o
	9.6 ± 0.3 , $p 3.0 \pm 1.0$, m
•	3.0 ± 0.6^{n}
$e 39.2 \pm 8.0^b$	$36.7,^h 32.3 \pm 3.2,^o$
	25.7 ± 1.5^{p}
	Environmental chamber studies ^{a,b} $\leq 2.3^{a}$ 2.5 ± 0.9^{a} 7.7 ± 2.3^{a} 14 ± 1^{a} 12.9 ± 2.6^{b} 7.4 ± 1.5^{a} 14 ± 3^{a} 20 ± 3^{a} 31 ± 4^{a} 2.0 ± 0.4^{b} 3.2 ± 0.6^{b} ant- 4.3 ± 0.9^{b} 3.8 ± 0.8^{b} 5.2 ± 1.0^{b} 17.5 ± 3.5^{b}

^a Reference 42. ^b From Table I. ^c Reference 40. ^d Reference 41. ^e Reference 21 for a mixture of xylene isomers. ^f Reference 24. ^g Reference 33. ^h References 30 and 21. ⁱ Reference 31. ^j Reference 36. ^k Reference 29. ^l Reference 28. ^m Reference 22. ⁿ Reference 32. ^o Reference 35. ^p Reference 34.

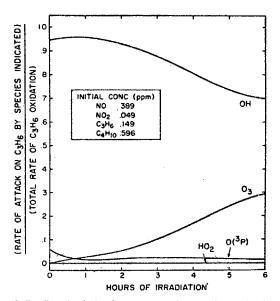


Figure 4. Predicted relative importance of several reactive intermediates during photooxidation of propene—n-butane mixture under simulated atmospheric conditions.

their reaction with ozone was necessary. For example, the rate constant for the reaction of ozone with toluene is about nine orders of magnitude lower than that for OH with toluene. During the initial hours of irradiation other species such as $\rm NO_3^{55}$ and $\rm HO_2^{56}$ may contribute slightly to hydrocarbon disappearance rates, especially for alkenes, but since their concentrations, and in some cases rate constants, are not known, correction was not possible.

Hydroxyl Radical Source in this System. The major sources of OH in our experimental system are probably the reactions^{7,8,13,15}

$$NO + NO_2 + H_2O \rightleftharpoons 2HONO \tag{2}$$

$$HONO + h\nu (290-410 \text{ nm}) \rightarrow OH + NO$$
 (3)

$$HO_2 + NO \rightarrow OH + NO_2$$
 (4)

Nitrous acid has been observed in a chamber study of simulated atmospheres carried out in our laboratory⁵⁷ when a mixture of propene and nitrogen oxides in moist air was photolyzed, indicating that HONO can be formed in HC/NO_x systems under conditions similar to those employed in the present study (Nash⁵⁸ claims to have measured HONO in ambient air, at levels up to 11 ppb). Direct evidence for formation of OH radicals in environmental chambers has been provided recently by Niki, Weinstock, and coworkers. ^{11,54} Reaction 4, of major importance, provides a further source of the OH radical. HO₂ can be formed in air^{56,59} by any mechanism producing H atoms or formyl radicals via the reactions

$$H + O_2 + M \rightarrow HO_2 + M \tag{5}$$

$$HCO + O_2 \rightarrow HO_2 + CO$$
 (6)

Thus any mechanism producing HO_2 in our system is also a means of furnishing OH radicals via reaction 4.

The concentration of OH radicals present during these experiments was calculated to be $(1.5-2.0) \times 10^6$ molecules cm⁻³ using the observed rates of m-xylene disappearance (corrected for dilution) and the previously determined rate constant for OH + m-xylene. $^{40.42}$ These concentrations are

of the same order as those observed directly in ambient $air^{10,11}$ as discussed above.

Aromatic Hydrocarbons. Present results for the rate constant for the reaction of OH with m-xylene show good agreement with the previous study⁴² carried out in our laboratory (Table II), indicating good reproducibility for this technique.

Rate constants for the reaction of OH with the propylbenzenes and ethyltoluenes have not been reported previously. However, the trend in rate constants for the reaction with o-, m-, and p-ethyltoluene is identical with that previously determined for the xylenes^{40,42} which supports the concept that OH is an electrophilic species, since attack on the meta compound is favored.

Davis et al.41 have studied the reaction of OH with benzene and toluene and from the observed pressure dependence of the reactions, conclude that addition occurs at least 50% of the time. In an environmental chamber study similar to that reported here, Schwartz et al.60 tentatively identified a number of aerosol products such as phenols and aromatic nitro compounds from the photooxidation of toluene in the presence of nitrogen oxides. A mechanism was proposed assuming initial addition of OH to the aromatic ring. In the case of the more highly substituted aromatic compounds studied here, it may be possible that hydrogen abstraction from the side chain could possibly be as important as addition. This is supported by the fact that a log plot of the OH-aromatic hydrocarbon rate constants vs. the ionization potential of the hydrocarbon (which, for abstraction reactions, is expected to be linear) in this case did not yield a straight line.

Detailed product studies are required in order to obtain the quantitative data necessary to further elucidate the mechanism of OH attack on various aromatic hydrocarbons.

Alkanes. Greiner²⁴ has derived an empirical formula for calculating the rates of reaction of OH with alkanes based on his experimental results for the reaction of the OH radical with selected alkanes:

$$k = 6.15 \times 10^8 N_1 \exp(-1635/RT)$$
+ 14.1 × 10⁸N₂ exp(-850/RT)
+ 12.6 × 10⁸N₃ exp(+190/RT) M⁻¹ s⁻¹

where N_1 , N_2 , and N_3 are the numbers of primary, secondary, and tertiary hydrogen atoms, respectively, in the alkane. We have used this equation to calculate the rate constants for isopentane, 2- and 3-methylpentane, and n-hexane. The calculated values are in quite good agreement with the experimental values. Although Greiner's formula predicts the same rate constants for the 2- and 3-methylpentanes, our study suggests that the latter is somewhat higher. Indeed this may be expected since the stability of the radical formed by the abstraction of the tertiary H atom from 3-methylpentane should be greater than that for the radical formed from similar attack in the 2-methylpentane case.

Alkenes. Unlike the alkanes and the aromatic compounds, alkenes react with ozone at a significant rate. Thus, in our experimental system, the small amounts of O_3 formed during the 3-h photolyses contributed to the alkene disappearance rates. From the measured concentrations of ozone and the published rate constants for the reaction of O_3 with the alkenes studied, $^{49,53,61-63}$ a correction was made to the alkene disappearance rates for loss due to reaction with ozone. This amounted to $\sim 3\%$ for ethene, $\sim 7\%$ for

propene, \sim 21% for cis-2-butene, and \sim 2% for 1,3-butadiene.

Our results for the reaction of OH with propene

$$OH + C_3H_6 \rightarrow products$$
 (7)

are within experimental error of a recent absolute determination of k_7 using flash photolysis-resonance fluorescence, 35 while the value of k_7 given in Table II for the result of \cos^{35} incorporates a stoichiometry factor of 2 to 3. In parallel studies in this laboratory using flash photolysis-resonance fluorescence 35 no evidence was found within experimental error of a pressure effect for k_7 by varying the total pressure from 25 to 100 Torr of argon, but additional studies should be carried out, especially at lower pressures where such an effect would become evident, to see whether k_7 exhibits any pressure dependence.

The value of the rate constant obtained in this study for the reaction of OH with cis-2-butene, though somewhat high, is within experimental error of values previously reported from direct determinations. ^{21,34,35} In this case a significant (21%) correction for reaction with O_3 had to be applied to the data.

No previous determinations of absolute rate constants have been reported for the reaction of OH with 1,3-butadiene. However, the close agreement between our values for cis-2-butene and 1,3-butadiene is consistent with the work by Cvetanovic and Doyle⁶⁴ who showed that these two compounds reacted at similar rates with oxygen atoms.

The value obtained in this study for the rate constant of the reaction

$$OH + C_2H_4 \rightarrow products$$
 (8)

of 5.2×10^9 M⁻¹ s⁻¹ is about a factor of 2 higher than published values from low pressure (<300 Torr) studies. 21,22,28-32,36 The only other study to date carried out at atmospheric pressure is that recently reported by Cox,33 in which OH was generated by photolyzing gaseous nitrous acid in nitrogen/oxygen mixtures (2:1) at 760 Torr and the effect of added alkenes on the photolysis of nitrous acid was studied. A rate constant $\alpha k_8 = (5.7 \pm 0.6) \times 10^9 \text{ M}^{-1}$ ${
m s}^{-1}$ was obtained relative to a value of $9.0 imes 10^7~{
m M}^{-1}~{
m s}^{-1}$ for the reaction of OH with CO, where α is a stoichiometry factor. Cox suggests that α is between 2 and 3 based on published values for the direct determination of k8. Davis et al.36 have shown that the significant differences between low pressure measurements of reaction 8 can be rationalized by the fact that the reaction exhibits a pressure dependence over the region studied (3 to 300 Torr of He).

This pressure dependence is probably due to the initial formation of the adduct observed by Niki and coworkers. ^{21,30} Presumably this adduct becomes stabilized by collisional deactivation

$$OH + C_2H_4 \xrightarrow{M} CH_2CH_2OH$$
 (8a)

While it is possible that our determination of k_8 is higher than previous values due to the fact that species other than OH and O_3 are depleting the ethene, at least part of the discrepancy may be due to the difference in pressure regions studied. Figure 5 shows a plot of $\log k_8$ vs. $\log P$ where P is the total pressure in the system for studies carried out using N_2 , O_2 , or N_2O as diluent gases. Studies carried out using less efficient third body gases such as He are not plotted since the present study is focused on ambient atmospheric conditions and third bodies such as N_2 or the

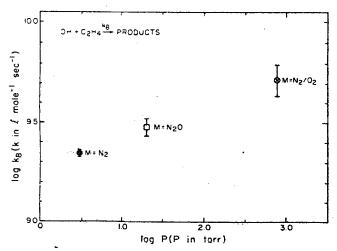


Figure 5. Variation with pressure of the rate constant k_8 for the reaction of OH with C_2H_4 ; M is "bath gas" in reaction 8: (\bullet) Davis et al.;³⁶ (\square) Smith and Zellner;³¹ (\otimes) this work.

equivalent. Thus, at 3 Torr of diluent gas, the results of Davis et al. 36 differ by a factor of 1.6 depending on whether N_2 or He is used as the diluent gas. Although our results for ethene are subject to some uncertainty, it appears possible that reaction 8 is not at the limiting high pressure kinetics region until the pressure exceeds 1 atm.

Conclusions

Relative rate constants have been determined for the reaction of OH with 14 hydrocarbons and these rate constants have been placed on an absolute basis using the literature values for the rate constant of OH + n-butane. No previous determinations have been reported in the case of seven of these compounds.

Our results indicate that the reaction of OH with ethene possibly does not obey second-order kinetics until pressures exceed 1 atm while for propene and the higher alkenes the reactions are second order at atmospheric pressure.

The comparatively high rates of reaction observed for the aromatic hydrocarbons have significant implications for the control of photochemical air pollution. This subject and the use of the present data in the formulation of a hydrocarbon reactivity scale has been treated in detail elsewhere.⁶⁵

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Relative Rate Constants for the Reaction of the Hydroxyl Radical with Selected Ketones, Chloroethenes, and Monoterpene Hydrocarbons

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The relative rates of disappearance of three monoterpene hydrocarbons, two chloroethenes, and three aliphatic ketones were measured in an environmental chamber under simulated atmospheric conditions at 305 \pm 2 K. The observed rates of disappearance were used to derive relative rates of reaction of these organic compounds with the hydroxyl radical (OH) on the previously validated basis that OH is the species dominantly responsible for the hydrocarbon disappearance under the experimental conditions employed. Absolute rate constants, obtained from the relative values using the published rate constant for OH + isobutene $(3.05 \times 10^{10} \, \mathrm{M}^{-1} \, \mathrm{s}^{-1})$, are $(k \times 10^{-10} \, \mathrm{M}^{-1} \, \mathrm{s}^{-1})$: α -pinene, 3.5 \pm 0.5; β -pinene, 4.1 \pm 0.6; d-limonene, 9.0 \pm 1.4; methyl ethyl ketone, 0.20 \pm 0.06 methyl isobutyl ketone, 0.9 \pm 0.3; diisobutyl ketone, 1.5 \pm 0.5; trichloroethene, 0.27 \pm 0.08; tetrachloroethene, 0.13 \pm 0.04. No previous determinations of these rate constants have been found in the literature. Rate constants for an additional nine monoterpene hydrocarbons have been derived from data recently published by Grimsrud, Westberg, and Rasmussen.

Introduction

During the last six years, the major role of the hydroxyl radical (OH) in atmospheric chemistry and photochemical air pollution has been recognized, 1-7 and kinetic data for the reaction of OH with both organic and inorganic species have increased substantially.8 However, there are currently no published rate constant determinations for the reaction of OH with ketones, chloroethenes, or any of the naturally occurring hydrocarbons such as the monoterpenes. Such rate constant data for the reaction of OH with these three classes of compounds would be useful in part because of their increasing importance for modeling the atmospheric processes occurring both in urban and rural atmospheres. Specifically, ketones and chlorinated hydrocarbons are components of commercial solvents.9,10 Both tri- and tetrachloroethene have been observed in the troposphere at part per trillion (ppt) concentrations of <511 and 20 ppt,11,12 respectively, while methyl ethyl ketone has been observed at concentrations of 1–6 parts per billion (ppb).¹³ Monoterpene hydrocarbons have been shown to be present in the atmosphere with source strengths of millions of tons annually.14 Thus, Rasmussen15,16 and coworkers have estimated that, on an individual basis, such naturally occurring hydrocarbons have ambient concentrations in the low ppb range and are largely responsible for the "blue haze" occurring in certain forested areas. 17

This paper describes an extension of our recent experiments in which an environmental chamber has been employed to obtain relative rate constants for the gas phase reaction of the hydroxyl radical with a series of hydrocarbons. ^{18,19} In this case we report data for the reaction of OH with three ketones, two chloroethenes, and three monoterpene hydrocarbons using isobutene as a reference compound.

Experimental Section

The experimental methods and procedures employed have been described in detail elsewhere 18,19 and are only briefly summarized here. Irradiations of the hydrocarbon- NO_x -air system were carried out in a Pyrex chamber 20 of approximately 6400-l. volume equipped with externally mounted

Sylvania 40-BL fluorescent lamps whose spectral distribution has been reported elsewhere 21 (photon flux at 300 nm is approximately 1% of the photon flux maximum at 360 nm). The light intensity, measured as the rate of NO₂ photolysis in nitrogen, $^{22}k_1$, was approximately 0.4 min⁻¹. All gaseous reactants were injected into pure matrix air 23 in the chamber using 100-ml precision bore syringes. Mixtures of the liquid reactants were injected using micropipettes. During irradiation, the chamber temperature was maintained at 305 ± 2 K.

Alkene, terpene, and ketone concentrations were measured by gas chromatography (GC) with flame ionization detection (FID) using the columns and techniques developed by Stephens and Burleson. ^{24,25} The chloroethenes were also monitored with GC(FID) using a 10 ft \times ½ in. stainless steel column packed with 10% Carbowax 600 on C22 Firebrick (100/110 mesh). Ozone ²⁶ was monitored by means of ultraviolet absorption (Dasibi Model 1003 analyzer), carbon monoxide by gas chromatography (Beckman 6800 air quality analyzer), and NO–NO₂–NO_x by the chemiluminescent reaction of NO with ozone (TECO Model 14B).

The initial concentrations of reactants are shown in Table I. In addition to these compounds, ethene (20–28 ppb), ethane (48–61 ppb), acetylene (25–37 ppb), propane (13–15 ppb), and variable concentrations of formaldehyde (16–134 ppb), acetaldehyde (0–7 ppb), and acetone (3–19 ppb) were present. Initial concentrations in these experiments were 1200–2100 ppb C of total nonmethane hydrocarbons, 0.58 ppm of NO_x (with an NO₂/NO_x ratio of 0.05–0.10), 5 ppm of CO, and 2900 ppb of methane, together with water vapor at 50% relative humidity. Replicate experiments were carried out in which this mixture was irradiated for 2–3 h with continuous analysis of inorganic species, analysis of hydrocarbons every 15 min, and analysis of monoterpenes, chloroethenes, and ketones every 30 min.

All data were corrected for losses due to sampling from the chamber by subtraction of the average dilution rate (1.2% per hour) from the observed hydrocarbon disappearance rate. The HC/NO_x and NO/NO_2 ratios were chosen to delay the formation of ozone, and ozone was not detected during the irra-

TABLE I: Rates of Disappearance and Rate Constants^a for Selected Ketones, Chloroethenes, and Monoterpene Hydrocarbons at 1 atm in Air at 305 ± 2 K

Initial concn, ppb	Relative rate of disap- pearance	$h_{ m OH},^b m M^{-1} \ s^{-1} imes 10^{-10}$
17-20 5-7 7-8 50-100	1.0 0.49 1.22 0.07	3.05 ± 0.31 1.49 ± 0.22 3.72 ± 0.56 0.20 ± 0.06
20-70	0.3	0.9 ± 0.3
20-32 10-20 10-20 10-20 41-161 14-88	0.5 1.14 1.33 2.95 0.088 0.044	1.5 ± 0.5 3.48 ± 0.52 4.06 ± 0.61 9.00 ± 1.35 0.27 ± 0.08 0.13 ± 0.04
	conen, ppb 17-20 5-7 7-8 50-100 20-70 20-32 10-20 10-20 10-20 41-161	Initial concn, disappearance 17-20 1.0 5-7 0.49 7-8 1.22 50-100 0.07 20-70 0.3 20-32 0.5 10-20 1.14 10-20 1.33 10-20 2.95 41-161 0.088

^a Placed on an absolute basis using 3.05×10^{10} M⁻¹ s⁻¹ for OH + isobutene from ref 35. ^b The indicated error limits are $\pm 15\%$, except in the case of the chloroethenes and ketones, for which they are $\pm 30\%$. These represent the estimated overall error limits and include both experimental errors and uncertainties which may occur in assuming that hydrocarbon disappearance is due solely to reaction with OH.

diation period, except in the case of one experiment, for which a small correction for the loss of hydrocarbon due to reaction with ozone was applied to the alkene disappearance rates.

In order to obtain additional data (at lower OH concentrations) to correct for the concurrent photolysis of the ketones as discussed below, irradiations of a mixture of ketones and isobutene were carried out. In these experiments, NO_x, CO, and other hydrocarbons were not added, and, under these conditions, relatively low concentrations of OH ($<5 \times 10^5$ radicals cm⁻³) were obtained.

Hydroxyl Radical Source in this System. As discussed previously, ¹⁹ the major sources of OH and its precursors in our experimental system are probably the reactions ^{4,5,27,28}

$$NO + NO_2 + H_2O \approx 2HONO$$
 (1)

$$HO_2 + NO_2 \rightarrow HONO + O_2$$
 (2)

$$HONO + h\nu (290-410 \text{ nm}) \rightarrow OH + NO$$
 (3)

$$HO_2 + NO \rightarrow OH + NO_2$$
 (4)

The first reaction is now thought to occur slowly homogeneously, ²⁹ but its rate is probably significantly faster when the reaction is catalyzed by surfaces. Thus, nitrous acid has been observed in a chamber study of simulated atmospheres carried out in our laboratory, ³⁰ while direct evidence for formation of OH radicals in an environmental chamber has been provided recently by Niki, Weinstock, and co-workers. ^{31,32}

Reaction 4, of major importance, provides a further source of the OH radical. HO₂ can be formed in air^{33,34} by any mechanism producing H atoms or formyl radicals (e.g., formaldehyde photolysis) via the reactions

$$H + O_2 + M \rightarrow HO_2 + M \tag{5}$$

$$HCO + O_2 \rightarrow HO_2 + CO$$
 (6)

Thus any mechanism producing HO_2 in our system is also a means of furnishing OH radicals via reaction 4.

The concentration of OH radicals present during these irradiated $HC-NO_x$ experiments was calculated to be (1.4-3.5)

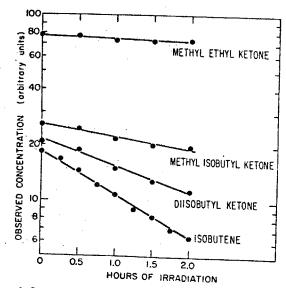


Figure 1. Concentrations of ketones (plotted on a logarithmic scale) during 2-h photolysis of HC–NO $_{\rm x}$ mixture in air at 305 \pm 2 K and 1 atm.

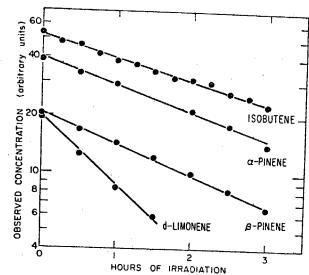


Figure 2. Concentrations of monoterpene hydrocarbons (plotted on a logarithmic scale) during 3-h photolysis of $HC-NO_x$ mixture in air at 305 \pm 2 K and 1 atm.

 \times 10⁶ radicals cm⁻³ using the observed rates of isobutene disappearance (corrected for dilution) and the previously determined rate constant for OH + isobutene.³⁵ These concentrations are of the same order as those observed directly in ambient air.^{31,32,36,37}

Results and Discussion

Typical rates of disappearance observed during a 2-h irradiation of the three ketones and 3-h irradiations of the three monoterpene hydrocarbons and the two chloroethenes are shown in Figures 1, 2, and 3, respectively. Isobutene was used as the reference compound (and is included in each figure), rather than n-butane which was used in our previous studies, 18,19 because its reactivity was closer to that of the terpenes, and its rate of decay could be measured more accurately in our system. In addition, the ratio of $k_{\rm OH}/k_{\rm O3}$ for isobutene is greater 32,35 than that for any of the other olefins studied, thus minimizing any contribution to the disappearance rate due to reaction with ozone. Table I gives the disappearance rates

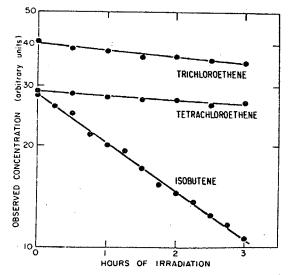


Figure 3. Concentrations of chloroethenes (plotted on a logarithmic scale) during 3-h photolysis of $HC-NO_x$ mixture in air at 305 \pm 2 K and 1 atm.

(corrected for dilution) for these reactants relative to that for isobutene based on data for the three separate experiments for monoterpenes and four separate experiments for methyl isobutyl and diisobutyl ketone and chloroethenes. Methyl ethyl ketone was present in all experiments.

Employing the fact that a range of OH concentrations (2.0 \times 10^5 –3.5 \times 10^6 radicals cm⁻³) was observed in these experiments, corrections to the measured rates of disappearance of the ketones were made for the possible small contribution from photolysis of these compounds. These corrections were made in the following manner. The observed rate of disappearance of a ketone is given by

$$d \ln \left[\text{ketone} \right] / dt = k_K [OH] + k_{h_\nu}$$
 (7)

where $k_{\rm K}$ and $k_{h\nu}$ are the rate constants for reaction with OH and photolysis, respectively. The isobutene disappearance rate is controlled solely by reaction with OH, hence

$$[OH] = \frac{d \ln [isobutene]}{dt \ k_{iB}}$$
 (8)

where k_{iB} is the rate constant for reaction of OH with isobutene. Thus, substituting for [OH] in eq 7

$$\frac{\mathrm{d} \ln \left[\text{ketone} \right]}{\mathrm{d}t} = \frac{k_{K}}{k_{\mathrm{iB}}} \frac{\mathrm{d} \ln \left[\text{isobutene} \right]}{\mathrm{d}t} + k_{h_{\nu}} \tag{9}$$

Based on eq 9, the relative rates of ketone disappearance were determined from the slopes of plots of d ln [ketone]/dt vs. d ln [isobutene]/dt. The intercepts of these plots gave the rate constants for photolysis. For methyl ethyl, methyl isobutyl, and diisobutyl ketone the ratios $k_{\rm K}/k_{\rm iB}$ were 0.07, 0.3, and 0.5, respectively, and the photolysis rate constants, $k_{h\nu}$, were 0.007, 0.014, and 0.25 h⁻¹, respectively.

On the basis that the OH radical is the species dominantly responsible for the hydrocarbon depletion during the 2- or 3-h irradiations (as discussed in detail in our earlier papers), 18,19 absolute rate constants were derived from the relative rates of disappearance using Atkinson and Pitts' value of $(3.05 \pm 0.31) \times 10^{10} \, \mathrm{M}^{-1} \, \mathrm{s}^{-1}$ for the reaction of OH with isobutene. These results are shown in Table I. It should be noted that the ratio of rate constants $(0.5 \, \mathrm{and} \, 1.2$, respectively) obtained here for propene and cis-2-butene relative to isobutene are in excellent agreement with the ratios obtained by Atkinson and Pitts $(0.5 \, \mathrm{and} \, 1.1$, respectively).

Ketones. To our knowledge, the data presented here represent the first experimental determination of rate constants for the reaction of the OH radical with any ketones in the gas phase. The only literature value for ketones is an estimated rate constant of $2.1 \times 10^9 \, \mathrm{M}^{-1} \, \mathrm{s}^{-1}$ for the reaction of OH with methyl ethyl ketone, which was made by Demerjian, Kerr, and Calvert⁵ on a thermochemical basis. This value is in remarkably good agreement with the experimental value obtained here $(2.0 \times 10^9 \, \mathrm{M}^{-1} \, \mathrm{s}^{-1})$.

The rate constants for the reaction of OH with the two other ketones reported here are significantly larger than that for methyl ethyl ketone. Thus, the rate constant for diisobutyl ketone is about the same as that for OH + propene. 8.19.35 The dominant mode of reaction of OH with ketones is expected to be one of hydrogen abstraction. This is consistent with the increased rate constant in going from methyl ethyl ketone to diisobutyl ketone reflecting a weaker C-H bond strength in going to more highly substituted ketone.

Acetone is relatively stable under conditions employed in our photooxidation studies, and, consequently, the rate constant for OH + acetone was not measured. Based on the fact that the C-H bond strength in acetone (98 kcal) is 6 kcal stronger than that for methyl ethyl ketone (92 kcal), one would expect OH to react significantly slower with acetone than with methyl ethyl ketone.

Chloroethenes. Rate constants for the gas phase reactions of OH with tri- and tetrachloroethene (C_2HCl_3 and C_2Cl_4 , respectively) have not been reported previously. The rate constants found in this study are 0.5 and 0.25, respectively, of the rate constant for OH + C_2H_4 . This difference in reactivity for the chloro-substituted ethenes and ethene is consistent with the results of Sanhueza and Heicklen, $^{38-40}$ who reported that the rates of reaction of $O(^3P)$ with C_2HCl_3 and C_2Cl_4 were the same and were both a factor of 10 less than that for the reaction of $O(^3P)$ with ethene.

Our results show that trichloroethene is more reactive with respect to attack by OH than tetrachloroethene. This is in agreement with the results of Lissi⁴¹ for CH₃O reactions and Franklin et al.⁴² for Cl atom reactions with these compounds. These workers found relative rates for attack on C_2HCl_3 and C_2Cl_4 of 2.2 and 2.6 for CH₃O and Cl, respectively, compared to 2.0 for OH, as found in the present study. Gay et al.⁴³ recently reported results from a photooxidation study of chloroethenes which, while not directly comparable to the present study due to the presence of substantial concentrations of ozone, showed that C_2HCl_3 disappeared more rapidly than C_2Cl_4 (near the beginning of their irradiations, when ozone concentrations were relatively low, the ratio of the rates of disappearance was \sim 2).

Since addition is likely to be the primary reaction pathway for attack by OH, the relative reactivity of C₂H₄, C₂HCl₃, and C₂Cl₄ should reflect the relative magnitudes of the ionization potentials of these molecules, which are 10.66, 9.48, and 9.34 eV, respectively. Our results are consistent with this trend.

Monoterpene Hydrocarbons. The terpenes experimentally investigated were α -pinene (I), β -pinene (II), and d-limonene (III). The detection limit for ozone in these experiments was

~1 ppb, and, since no ozone was detected during irradiations of the terpenes, an upper limit to the contribution due to reaction with ozone to the observed rates of terpene disap-

TABLE II: Reactivity of Selected Monoterpenes with O(3P), O₃, and OH

	Rate constant, M ⁻¹ s ⁻¹		
Compound	O(3P)2	О,	OHe
α-Pinene	1.60 ± 0.06 × 10 ¹⁰	$2.0 \times 10^{s}, b$ 1.0×10^{sc} 8.8×10^{sd}	3.5 × 1010
β-Pinene	1.51 ± 0.06 × 10 ¹⁰	$2.2 \times 10^{+d}$	4.1 × 1010
d-Limonene	6.50 ± 0.52 × 10 ¹⁰	$3.9 \times 10^5 d$	9.0 × 10 ¹⁰

^a Reference 49. ^b Reference 48. ^c Reference 45. ^d Reference 16. ^e This work.

pearance can be calculated. Thus, assuming an ozone concentration of ≤ 1.0 ppb, and using published rate constants for the reaction of ozone with the terpenes, $^{16.43-45}$ an upper limit of 7% of the overall disappearance rate is obtained for the case of d-limonene (the worst case) at the lowest OH concentration present in these experiments (1.4 \times 10⁶ radicals cm⁻³).

It is interesting to note that the rate constant, 3.7×10^{10} M⁻¹ s⁻¹, obtained in this study for OH + cis-2-butene, a component in the hydrocarbon mix (Table I) used in this set of experiments, is in good agreement with the values of 3.2×10^{10} and 3.7×10^{10} M⁻¹ s⁻¹, obtained by Atkinson and Pitts³⁵ and Morris and Niki,⁴⁶ respectively, although our value is somewhat higher than the value of 2.6×10^{10} M⁻¹ s⁻¹ obtained by Fischer et al.;⁴⁷ in these three studies, the rate constant was determined from elementary reaction measurements.

Table I shows the absolute rate constant values obtained for the terpenes. Clearly, these natural hydrocarbons react very rapidly with OH. For example, α -pinene reacts about 3×10^5 times faster with OH than with ozone. And Thus, for an ozone concentration of 3×10^{12} molecules cm⁻³ (0.12 ppm) and an OH concentration of 10^7 radicals cm⁻³, the rates of disappearance of α -pinene due to reaction with O_3 and OH, respectively, will be essentially equal. A comparison of the rates of the three terpenes with $O(^3P)$, O_3 , and OH is given in Table II. 16,45,46 Within the experimental errors for the rate constants for OH + α - and β -pinene, the trend observed for reaction with OH is the same as that observed for reaction with $O(^3P)$ and O_3 .

Grimsrud, Westberg, and Rasmussen (GWR)¹⁶ have reported the relative rates of photooxidation of a series of monoterpene hydrocarbons using mixtures of 10 ppb of the monoterpene and 7 ppb of nitric oxide, which were irradiated for periods ranging between 60 and 120 min. Making the reasonable assumption that, as in the case of our studies, OH is the major species depleting the hydrocarbon in their experiments, then a series of rate constants relative to isobutene (which was included in the GWR study) can be generated in the same manner as described above. The data from GWR are given in Table III relative to isobutene = 1.0.

Considering the uncertainties involved in this approach (including a lack of knowledge of the exact ozone concentrations formed in the experiments of GWR), the agreement between our results for the reaction of OH with α - and β -pinene and d-limonene and those shown in the fourth column of Table III is quite good and, except in the case of α -pinene, well within the estimated experimental uncertainty for our determinations. The fact that our value of OH + d-limonene is only slightly higher than GWR suggests that little or no O3 was formed in their experiments, since there was less than 1 ppb formed during our irradiations.

TABLE III: Relative Reaction Rates of Monoterpene Hydrocarbons and Rate Constants^a for Their Reaction with the OH Radical Based on Data from Grimsrud, Westberg, and Rasmussen (Ref 16)

Hydrocarbon	Structure	Rel reactivity	$_{\rm s^{-1} \times 10^{-10}}^{k_{ m OH}, \ { m M^{-1}}}$
p-Menthane	-	0.13	0.40
p-Cymene	\leftarrow	0.30	0.92 (0.78 ± 0.16)
Isobutene	>	1.0	3.05
β-Pinene	$\times \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \!$	1.3	4.0 (4.1 ± 0.6)¢
Isoprene	>	1.5,	4.7 (4.6 ± 0.9)d
α-Pinene	$\times\!$	1.5 ₅	4.7 (3.5 ± 0.5)c
3-Carene	-\frac{1}{2}	1.7	5.2
β -Phellandrene	$\overline{}$	2.3	7.0
Carvomenthene	$\overline{}$	2.5	7.6
d-Limonene	$-\!$	2.9	8.8 (9.0 ± 1.4) ^c
Dihydromyrcene	$\rightarrow \searrow$	3.6	10.1
Myrcene		4.5	13.7
cis-Ocimene	\rightarrow	6.3	19.2

^a Placed on an absolute basis using 3.05×10^{10} M⁻¹ s⁻¹ for OH + isobutene from ref 35. ^b For p-ethyltoluene which is structurally similar (ref 19). ^c Present work (see Table II). ^d For 1,3-butadiene which is structurally similar (ref 19).

A further check on the validity of using the results of Grimsrud, Westberg, and Rasmussen¹⁶ to obtain OH rate constant data is provided by the values derived for the reaction of OH with p-cymene and isoprene, p-Cymene is structurally very similar to p-ethyltoluene, and hence the OH rate constants for these two compounds should be comparable. In fact, this is the case with the value for OH + p-cymene of $9.1 \times 10^9 \,\mathrm{M}^{-1} \,\mathrm{s}^{-1}$ derived from the data of GWR being very close to that obtained for OH + p-ethyltoluene, $7.8 \times 10^9 \,\mathrm{M}^{-1}$ s⁻¹, in our previous study. 19 Likewise, isoprene is structurally similar to 1,3-butadiene, and the rate constant derived for isoprene of $4.7 \times 10^{10} \ \mathrm{M^{-1} \ s^{-1}}$ is consistent with that previously measured 19 for OH + 1,3-but adiene of $4.6 \times 10^{10} \, \mathrm{M}^{-1}$ s⁻¹. On the basis of these comparisons, it appears valid to use the photooxidation data of Grimsrud, Westberg, and Rasmussen16 to obtain OH rate constant data for the series of monoterpenes which they investigated.

Conclusion

Relative rate constants have been experimentally determined for the reaction of OH with eight compounds, and these rate constants have been placed on an absolute basis using the literature value for the rate constant for OH + isobutene. In the same manner, rate constants for the reaction of OH with nine additional compounds (monoterpene hydrocarbons) for

which no previous rate constants are available have been derived from data recently published by Grimsrud, Westberg, and Rasmussen.16

The comparatively large rate constants obtained for the ketones and monoterpene hydrocarbons indicate that they will be quite reactive in the troposphere. The implications for photochemical oxidant control strategies of the chemical reactivity of the ketones, chloroethenes, and terpenes are discussed in detail elsewhere.50,51

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Reactivity Scale for Atmospheric Hydrocarbons Based on Reaction with Hydroxyl Radical

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By use of relative and absolute rate constants for the reaction of the hydroxyl radical (OH) with a number of alkanes, alkenes, aromatics, and ketones, a reactivity scale is formulated based on the rate of removal of hydrocarbons and oxygenates by reaction with OH. In this five-class scale, each class spans an order of magnitude in reactivity relative to methane. Thus, assigned reactivities range from <10 for Class I (containing only methane) to >104 for Class V containing the most reactive compounds (e.g., d-limonene). This scale differs in several significant ways from those presently utilized by air pollution control agencies and various industrial laboratories. For example, in contrast to other scales based on secondary manifestations such as yields of ozone and eye irritation, it focuses directly on initial rates of photooxidation. The proposed scale also provides a clearer understanding of the importance of alkanes in the generation of ozone during periods of prolonged irradiation. The present scale can be readily extended to include additional organic compounds (e.g., natural and anthropogenic hydrocarbons, oxygenates, chlorinated solvents), once their rate of reaction with OH is known.

It has been recognized for many years (1-21) that all hydrocarbons occurring in polluted atmospheres are not equally effective in producing photochemical oxidant, and hence that the application of cost effective strategies for the control of hydrocarbons requires that more stringent emissions reductions be applied to the more reactive organic compounds (22-25). This in turn has led to a continuing requirement for a rational assessment of hydrocarbon reactivity as a basis for control decisions. Such an assessment is particularly critical since attainment of the Federal air quality standard for photochemical oxidant has been sought largely through the stringent control of hydrocarbon emissions (26-27).

The first effort to formulate and apply a practical hydrocarbon reactivity scale was taken in 1966 with the implementation by the Los Angeles Air Pollution Control District (LAAPCD) of a regulation, known as Rule 66, to limit solvent organic emissions on the basis of their capacity for promoting photochemical smog formation (24–25). This rule and other conceptions of reactivity scales (28) represented a major advance in the application of the information then available concerning the mechanisms of photochemical smog formation to the development of practical air pollutant emission control strategies.

Not surprisingly however, both in the past and present, there have been significant differences in hydrocarbon reactivity scales proposed by local, regional, and national air pollution control agencies (23, 29-31) as well as by industry (14, 16). As shown in Table I, this can lead to very large differences in emission inventory estimates and in approaches to hydrocarbon control (29, 32, 33). In this case, reactive hydrocarbon emission inventory levels calculated by Goeller et al. (32) using hydrocarbon reactivity definitions of the Environmental Protection Agency (EPA) on the one hand, and the California Air Resources Board (ARB) and LAAPCD on the other, differed by factors of 3 to 4!

A second problem common to virtually all previous reactivity classifications has been their reliance on smog chamber data obtained for relatively short irradiation (~2-6 h) periods.

Thus, the recent concern over oxidant formation resulting from longer irradiations during pollutant transport to regions downwind of urban sources introduces additional difficulties both in defining what constitutes a reactive hydrocarbon and in categorizing degrees of reactivity. For example, a compound such as propane, the major component in liquefied petroleum gas (LPG) and often cited as a "clean" fuel, is now known (34–36) to contribute to the formation of photochemical oxidants in the later stages of day-long irradiation periods. However, on the basis of data obtained during short-term irradiations, propane has been classified as "unreactive" in a reactivity scale proposed (23) by B. Dimitriades of the EPA (hereafter referred to as the EPA reactivity scale).

Altshuller and Bufalini (9, 17) have reviewed the various definitions of hydrocarbon reactivity and summarized results of numerous studies up to 1970. The criteria used for evaluating hydrocarbon reactivity include hydrocarbon consumption, the conversion of nitric oxide to nitrogen dioxide, ozone formation, aerosol formation, eye irritation, and plant damage. It is generally agreed that the criteria most suitable with respect to photochemical oxidant control strategies are ozone dosage or maximum ozone concentration (29). However, establishing a definitive hydrocarbon reactivity scale to be applied specifically to the control of ozone formation requires an extensive and lengthy experimental program in which the ozone-forming capability of each individual hydrocarbon is determined under simulated atmospheric conditions, including long-term irradiation (i.e., 12–14 h).

An alternative basis for assessing hydrocarbon reactivity, which would appear to have considerable utility and a valid experimental foundation, is the formulation of a reactivity scale based on the rate of disappearance of hydrocarbons due to reaction with the hydroxyl radical, the key intermediate species in photochemical air pollution.

Results and Discussion

It is only in the last six years that the critical role of OH in photochemical smog formation has been generally recognized (37-40) and that appreciable rate constant data have become available for the reaction of OH with several classes of hydrocarbons. The importance of OH as a reactive intermediate relative to species such as O_3 , $O(^3P)$, and HO_2 has been shown previously (39-41) through computer modeling of smog chamber data. For example, Niki et al. (39) showed that the reactivity of a number of hydrocarbons, as measured by the rate of conversion of NO to NO₂, correlated significantly better with OH rate constants than with either $O(^3P)$ or O_3 rate constants.

Table I. Comparison of Reactive Hydrocarbon Inventory Levels for Fixed Sources Under Alternative Reactivity Assumptions (from Ref. 32 Based on Pre-1973 Data)

	Reacti	ve hydrocarbons, t	ons/day
Control strategy	Consistent EPA	ARB- LAAPCD	Rand Corp.
1970	876.0	228.3	636.3
1975 nominal	427.3	102.2	239.9
1975 maximal	290.6	57.7	129.9

The utility of a large environmental chamber in obtaining relative rate constants with an accuracy of ±20% for the reaction of the hydroxyl radical with a variety of hydrocarbons was demonstrated in an earlier study in this laboratory (41). This method has recently been extended to an investigation of more than a dozen additional hydrocarbons, including seven compounds for which OH rate constants are not currently available. The detailed kinetic data derived from this investigation have been reported elsewhere (42). In these studies we determined the relative rates of disappearance of selected alkanes, alkenes, and aromatic hydrocarbons under simulated atmospheric conditions of temperature, pressure, concentrations, light intensity, and other trace contaminants (NOx, CO, hydrocarbons, water). These relative rate constants were placed on an absolute basis using the published rate constants for OH + n-butane. The assumption that OH was responsible for the hydrocarbon disappearance under the experimental conditions employed (41) was subsequently supported by the very good agreement between OH rate constants determined for the individual compounds using flash photolysis-resonance fluorescence techniques (43, 44) and those obtained in the initial chamber study (41). The general validity of the chamber method for obtaining OH rate constants is illustrated in Figure 1 where the good correspondence between chamber values (41, 42) and the available literature values [(45) and references in Table IV] is shown graphically.

The importance of the chamber method for the purposes of formulating a reactivity scale is the simultaneous determination of valid rate constants for reactions of OH with a large number and wide variety of atmospherically important hydrocarbons. This substantially expands the number of compounds which can be incorporated, now and in the near future, in the resulting reactivity scale. In this regard we are currently extending (46) the chamber method to the determination of rate constants for reactions of OH with natural hydrocarbons, such as terpenes, and solvent hydrocarbons, such as ketones and chloroethenes, for which no data currently exist. Preliminary kinetic data (46) for selected natural hydrocarbons and ketones are included in our proposed reactivity scale.

Use of OH Rate Constants as a Reactivity Index. From the successful correlation of OH rate constants with the rates of hydrocarbon disappearance observed in our chamber simulations, we conclude that, to a good approximation, this

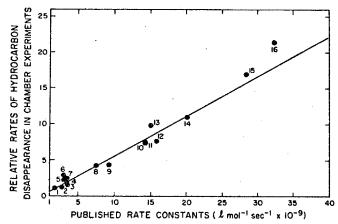


Figure 1. Comparison of relative rates of hydrocarbon disappearance determined by environmental chamber method (refs. 41 and 42) with selected published rate constants (cited in Table IV) for reaction of those hydrocarbons with OH radicals

Line shown represents one to one correspondence and has slope of $(1/1.8) \times 10^{-9}$ mol s l. $^{-1}$. Compounds shown are: 1, r-butane; 2, isopentane; 3, toluene; 4, 2-methylpentane; 5, r-hexane; 6, ethene; 7, 3-methylpentane; 8, p-xylene; 9, o-xylene; 10–11, m-xylene; 12, 1,2,3-trimethylbenzene; 13, propene; 14, 1,2,4-trimethylbenzene; 15, 1,3,5-trimethylbenzene; 16, cis-2-butene

Table II. Effect of 0.1 PPM Ozone on Calculated Lifetimes of Selected Alkenes Based on Reaction with OH Radicals (1×10^7 Radicals/cm³) ^a at 300 K

Alkene	OH rate constants, b i, mol ⁻¹ s ⁻¹	Half-life c for $[O_3] = 0$, h	Half-life d for $[O_3] = 0.1$ ppm, h
Ethene	3.8×10^{9}	3.0	2.8
Propene	1.5×10^{10}	0.76	0.67
cis-2- Butene	3.2×10^{10}	0.36	0.20
1,3-Buta-	4.6×10^{10}	0.25	0.24

^a Concentration used in these calculations—see text. ^b See references in Table IV. ^c $t_{1/2}=0.693/k_{\rm OH}[{\rm OH}]$ under the assumption of attack only by OH. ^d $t_{1/2}=0.693/(k_{\rm OH}[{\rm OH}]+k_{\rm O_3}[{\rm O_3}]);~k_{\rm O_3}$ taken from refs. 45 and 59.

correlation can be extrapolated to the atmosphere for alkenes in ambient air parcels during the early morning hours when ozone levels are generally quite low (≤ 0.05 ppm), and for alkanes and aromatics at essentially all times and locations. The latter assumption, namely, that an OH rate constant is a good "reactivity index" for alkanes and aromatics throughout an irradiation day (or multiple irradiation days), rests upon the fact that the rates of reaction of these classes of hydrocarbons with species such as ozone, $O(^3P)$ atoms, and hydroperoxyl radicals are several orders of magnitude slower than with OH (45, 47–49). For example, even at the highest ozone concentrations experienced in ambient atmospheres, O_3 will not contribute significantly to the photooxidation of alkanes and aromatics.

This is in contrast to the case for alkenes which, although the rate constants for reaction of O₃ with alkenes are not particularly large (45), react rapidly with ozone at the average concentrations commonly encountered in polluted ambient air (~0.1-0.2 ppm). The approximate magnitude of the effect of ozone on the atmospheric lifetimes of alkenes is given in Table II. From their OH rate constants (see Table IV), atmospheric lifetimes for four alkenes were obtained by assuming an OH radical concentration in polluted atmospheres of 107 radicals cm⁻³, which is a reasonable value on the basis of both model calculations (50) and recent atmospheric measurements (51-53). The half-life given in column 3 of Table II is defined as $t_{1/2} = 0.693/k(OH)$, and assumes depletion of the hydrocarbon solely by the hydroxyl radical. When one assumes an average concentration of 0.10 ppm of O₃, the more reactive alkenes show considerably shorter half-lives (column 4). For example, the lifetime of cis-2-butene in the atmosphere is 0.36 h assuming only reaction with OH. but this is reduced to 0.20 h when reaction with O3 at a concentration of 0.1 ppm is considered.

Proposed Reactivity Scale. Under the assumption that hydrocarbon depletion is due solely to attack by OH (with the qualification noted for alkenes), we propose a five-class reactivity scale based on hydrocarbon disappearance rates due to reaction with OH. The ranges of reactivities for the five proposed classes each span an order of magnitude in reactivity relative to methane and are shown in Table III. The hydrocarbon half-lives, as defined above, are also shown for each reactivity range.

Hydroxyl radical rate constant data for a wide range of atmospheric hydrocarbons have been taken from the literature as well as from our own studies and are compiled and referenced in Table IV. The assignment of these compounds in the various classes of our proposed reactivity scale is shown in the last column of Table IV. For interest, carbon monoxide is included in this table since, although it is not a hydrocarbon, it is present in polluted urban atmospheres but is generally regarded as being "unreactive" in ambient air. Thus, carbon

monoxide appears as being somewhat reactive in Class II, which also includes ethane and acetylene. In our current compilation of compounds, methane is the only compound listed which appears in Class I, and 2-methyl- and 2,3-dimethyl-2-butene and d-limonene are the only compounds in Class V. Several of the higher alkenes and 1,3-butadiene appear at the upper end of Class IV. Data from our recent study of monoterpene hydrocarbons (46) indicate that many of these compounds will appear in Class V (54).

Comparison with Other Scales. The ranking of reactivities for the aromatic hydrocarbons in our scale is essentially the same as that obtained by Altshuller et al. (4) and by Kopczynski (7, 17). Although our proposed scale is based solely on hydrocarbon disappearance rates, Altshuller and Bufalini (17) have shown that this measure of reactivity is very similar to the one based on nitric oxide oxidation rates. They showed that the ranking of reactivities of hydrocarbons from the nitric oxide photooxidation studies of Altshuller and

Table III. Reactivity Scale for Hydrocarbons Based on Rate of Disappearance of Hydrocarbon Due to Reaction with Hydroxyl Radicals

Class	Half-life.	Reactivity rel to methane (=1)
1	>9.9 days	<10
II.	24 h to 9.9 days	10–100
111	2.4-24 h	100-1000
١٧	0.24-2.4 h	1000-10 000
V	<0.24 h	>10 000
$a t_{1/2} = 0$.693/k _{OH} [OH].	

Cohen (6) and Glasson and Tuesday (8) was essentially the same as that obtained from the studies of hydrocarbon consumption carried out by Schuck and Doyle (1), Stephens and Scott (3), and Tuesday (5). We are currently investigating methods of quantitatively relating hydrocarbon consumption to nitric oxide oxidation and ozone formation, the parameter of greatest interest in formulating control strategies for oxidant reduction.

As indicated above, Rule 66 formulated by the LAAPCD in 1966 represented the first hydrocarbon control measure based on photochemical reactivity. Although this regulation has been effective, results from recent studies (34–36) indicate that the 4–6 h irradiations (25), from which assignments of the degree of reactivity of hydrocarbons were made in formulating Rule 66, did not give sufficient recognition to the ozone-forming potential of slow reactors such as n-butane and propane. Consequently, it is now realized that measures more stringent than Rule 66 are necessary to achieve reductions in ozone formation to levels approaching those mandated by the U.S. Clean Air Act Amendments of 1970.

Recognition of such deficiencies in current hydrocarbon control regulations has led to reexamination of present hydrocarbon reactivity classifications. The focus of these reevaluations has been the five-class reactivity scale (see Table V) proposed by B. Dimitriades at the EPA Solvent Reactivity Conference in 1974 (23). Significant changes have been suggested for this reactivity classification by the California ARB (29, 30), the LAAPCD (31), the EPA (55), and by industry. However, since no final conclusions have been reached by any of these agencies at this time, we will restrict comparison of our proposed scale to the 1974 EPA scale.

Table IV. Proposed Reactivity Classification of Hydrocarbons and CO Based on Reaction with Hydroxyl Radicals

Compound	$k_{\rm OH} + {\rm Cpd} \; ({\rm i. \; mol}^{-1} \; {\rm s}^{-1}) \times 10^{-9}$	Ref#	Reactivity rel to methane	Proposed class, see Table III
Methane	0.0048	(60)	1	l
CO	0.084	(45)	18	in ·
Acetylene	0.11	(45, 61, 66)	23	ii
Ethane	0.16	(62)	33	i
Benzene	0.85	(43, 44)	180	 IN
Propane	1.3	(63)	270	111
n-Butane	1.8	(41, 42)	375	 Bi
Isopentane	2.0	(42)	420	in
Methyl ethyl ketone	2.1	(46)	440	iii
2-Methylpentane	3.2	(42)	670	iii
Toluene	3.6	(43, 44)	750	111
n-Propylbenzene	3.7	(42)	770	111
Isopropylbenzene	3.7	(42)	770	111
Ethene	3.8	(42, 64-66)	790	111
<i>n</i> -Hexane	3.8	(42)	790	111
3-Methylpentane	4.3	(42)	900	III
Ethylbenzene	4.8	(42)	1000	 !!!–!V
<i>p</i> -Xylene	7.45	(41, 43)	1530	IV
<i>p</i> -Ethyltoluene	7.8	(42)	1625	IV
o-Ethyltoluene	8.2	(42)	1710	IV
o-Xylene	8,4	(41, 43)	1750	IV
Methyl isobutyl ketone	9.2	(46)	1920	iv
<i>m</i> -Ethyltoluene	11.7	(42)	2420	iv
<i>m</i> -Xylene	14.1	(41, 43)	2920	iv
1,2,3-Trimethylbenzene	14.9	(41, 43)	3100	IV
Propene	15.1	(67)	3150	IV
1,2,4-Trimethylbenzene	20	(41, 43)	4170	iV
1,3,5-Trimethylbenzene	29.7	(41, 43)	6190	iv
cis-2-Butene	32.3	(67)	6730	iv
eta-Pinene	42	(46)	8750	iv
1,3-Butadiene	46.4	(42)	9670	IV-V
2-Methyl-2-butene	48	(68)	10 000	v
2,3-Dimethyl-2-butene	67	(69)	14 000	v
d-Limonene	90	(46)	18 800	v
* Where more than one referen	ice is cited an average value is given for the			-

Where more than one reference is cited, an average value is given for the rate constant.

Table V. Proposed EP/	Reactivity Classification of	f Organics (f	rom Ref. 2	23, 1974)
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Class I, nonreactive	Class II, reactive	Class III, reactive	Class IV, reactive	Class V, reactive
C1-C3 paraffins Acetylene Benzene Benzaldehyde Acetone Methanol Tertiary-alkyl alcohols Phenyl acetate Methyl benzoate Ethyl amines Dimethyl formamide Perhalogenated hydrocarbons	Mono-tertiary- alkyl benzenes Cyclic ketones Tertiary-alkyl acetates 2-Nitropropane	C ₄₊ paraffins Cycloparaffins Styrene n-Alkyl ketones Primary and secondary alkyl acetates N-methyl pyrrolidone N,N-dimethyl acetamide Partially halogenated paraffins Paraffins	Primary and secondary alkyl benzenes Dialkyl benzenes Branched alkyl ketones Primary and secondary alkyl alcohols Cellosolve acetate Partially halogenated olefins	Aliphatic olefins α-Methyl styrene Aliphatic aldehydes Tri- and tetra-alkyl benzenes Unsaturated ketones Diacetone alcohol Ethers Cellosolves
Reactivity rating: 1.0	3.5	6.5	9.7	14.3

Briefly, the EPA has proposed, on the basis of previous experimental studies, that methane, ethane, acetylene, propane, and benzene are essentially nonreactive for typical urban ambient hydrocarbon– NO_{κ} ratios (23) and these compounds are placed in Class I on their scale. Three other classes have been proposed for mobile source hydrocarbon emissions (56)—Class III (C₄ and higher alkanes), Class IV (aromatics less benzene), and Class V (alkenes). When stationary source hydrocarbons, including solvents (Class II), are added to the list, five classes are suggested as shown in Table V.

The reactivity classification proposed here (Tables III and IV) can be compared with that suggested by the EPA (Table V). It is evident that several significant differences emerge:

- The C₁-C₃ alkanes are given equal weighting in the EPA scale, and all are designated unreactive, whereas our scale clearly differentiates among the three compounds from methane in Class I and ethane in Class II to the more reactive propane in Class III.
- According to our proposed classification, benzene and n-butane are of similar reactivity, whereas the EPA scale places them in Class I and III, respectively.
- All the alkenes are placed in Class V of the EPA scale, whereas our proposed scale shows a differentiation in reactivity from ethene in Class III to 2,3-dimethyl-2-butene in Class V.
- Our scale gives recognition to the high reactivity of natural hydrocarbons such as β -pinene and d-limonene, placing these in Class IV and V, respectively. The present published EPA scale does not give a classification for natural hydrocarbons, although they could be loosely categorized as substituted alkenes in Class V.

In addition to noting these differences, some similarities exist between the two scales. For example, our scale shows that 1,3-butadiene is highly reactive which is consistent with previous studies indicating it to be a facile precursor of eye irritants (17) and highly effective in producing oxidant during irradiation of HC-NO_x mixtures (57). Also, methanol would appear in the low half of Class II in our scale based on a recent determination of the rate constant for OH attack on methanol (58). The value found was $k_{(OH+CH_3OH)}/k_{(OH+CO)} = 0.63$ at 298 K. This reduces to 5.3×10^7 l. mol⁻¹ s⁻¹ based on $k_{(OH+CO)} = 8.4 \times 10^7$ l. mol⁻¹ s⁻¹ (45). Hence, both our scale and the EPA's show methanol to be relatively unreactive.

It should be emphasized that the classification proposed in our scale is not strictly applicable to compounds which undergo significant photodissociation in the atmosphere, for example, aliphatic aldehydes. In such cases, the compound will be more reactive than predicted from a scale based on hydrocarbon depletion due solely to OH attack. However, our proposed classification emphasizes that most compounds react in polluted atmospheres and suggests that the Class I scale be reserved only for the few compounds which have half-lives greater than about 10 days.

Conclusion

Our proposed reactivity scale based on the depletion of hydrocarbons by reaction with the OH radical has utility in assessing hydrocarbon chemical behavior in polluted ambient air. Since only those organic compounds which participate in atmospheric reactions are of consequence in the chemical transformations in ambient air, their relative reactivity toward OH is a useful and directly measurable index of their potential importance in the production of secondary pollutants.

One advantage of the proposed scale is that, because it is based on the individual rate constants for hydrocarbon reaction with OH, any degree of gradation in reactivity may be used to formulate any desired number of classes—from relatively few to a large number of classes or even an ordered ranking of compounds. A second strength of the present scale is that it can be readily extended to include additional organic compounds once their rate of reaction with OH is known. Finally, the proposed scale gives greater weight than previous reactivity scales to the alkanes and a number of aromatic hydrocarbons, which require a longer period of time to react but can contribute significantly to ozone formation during longer irradiation periods, e.g., during their transport downwind from urban centers—a phenomenon of increasing concern to air pollution control agencies.

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DEVELOPMENT AND APPLICATION OF A HYDROCARBON REACTIVITY SCALE BASED ON REACTION WITH THE HYDROXYL RADICAL

bу

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Abstract

Measurements of the relative rate constants for the reaction of the hydroxyl radical (OH) with some 35 atmospherically important hydrocarbons have been made in the SAPRC 6400 & glass irradiation chamber. These rate constants were placed on an absolute basis using literature values for either n-butane or isobutene and have been augmented with OH rate data obtained by elementary reaction measurements and other appropriate data, such as that from photo-oxidation studies, from which relative and absolute OH rate constants could be calculated.

Utilizing these data, a reactivity scale for some 80 compounds, including alkenes, alkanes, aromatics, oxygenates, and naturally occurring hydrocarbons, has been formulated based on the removal of the hydrocarbons by reaction with OH. The resulting scale is an ordering of the reactivities of the hydrocarbons relative to methane. The scale can be divided into an arbitrary number of classes for purposes of application to control strategies or comparison with other reactivity scales.

Some comparisons of the present scale with proposed EPA and ARB reactivity scales are made, and the implications of the present scale for the role of alkanes and a number of aromatic hydrocarbons in the formation of ozone in regions downwind of urban centers is analyzed.

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Introduction

A major result of the photooxidation studies of the past 20 years \$^{1-26}\$ has been the recognition that atmospherically important hydrocarbons do not all contribute equally to the production of photochemical oxidant, and hence that the application of cost effective strategies for the control of hydrocarbons requires that more stringent emissions reductions be applied to the more reactive organic compounds. \$^{10,11,19,26}\$ This in turn has led to a continuing requirement for a rational assessment of hydrocarbon reactivity as a basis for control decisions. Such an assessment is particularly critical since attainment of the Federal air quality standard for photochemical oxidant has been sought largely through the stringent control of hydrocarbon emissions. \$^{27,28}\$

The first effort to formulate and apply a practical hydrocarbon reactivity scale was taken in 1966 with the implementation by the Los Angeles Air Pollution Control District (LAAPCD) of a regulation, known as Rule 66, to limit solvent organic emissions on the basis of their capacity for promoting photochemical smog formation. 10,11 This rule and other conceptions of reactivity scales 29 represented a major advance in the application of the information then available concerning the mechanisms of photochemical smog formation to the development of practical air pollutant emission control strategies. Thus, the basic concept of selective control of emissions based on their reactivity is now widely established.

Not surprisingly however, there have been significant differences in hydrocarbon reactivity scales proposed by local, regional, and national air pollution control agencies 25 , $^{30-34}$ as well as by industry. 16 , 18 , 23 This in turn can lead to quite large differences in emission inventory estimates and in approaches to hydrocarbon control. 30 , 35 , 36

Most, although not all, previous reactivity classifications have relied primarily on smog chamber data obtained for relatively short irradiation (≤ 6 hrs) periods. Thus, the recent concern over oxidant formation resulting from longer irradiations during pollutant transport to regions downwind of urban sources introduces additional difficulties both in defining what constitutes a reactive hydrocarbon and in categorizing degrees of reactivity. For example, a compound such as propane, the major component in liquified petroleum gas (LPG) and often cited as a "clean" fuel, is now known³⁷⁻³⁹ to contribute to the formation of photochemical oxidants in the later stages of day-long irradiation periods. However, on the basis of data obtained during short-term irradiations, propane has been classified as "unreactive" in a reactivity scale

proposed²⁵ in 1974 by B. Dimitriades of the EPA (hereafter referred to as the EPA reactivity scale).

A third difficulty with reactivity scales which are based on previous smog chamber data concerns their reliance on measurements of smog manifestations such as maximum ozone concentrations. Observed values of such secondary properties of a photooxidation system can be significantly affected by the particular chamber materials, light source, purity of matrix air, and other aspects of the chamber methodology employed. This fact can account in large measure for the significant number of discrepancies which arise from comparison of the specific ranking of hydrocarbons in reactivity scales formulated on the basis of different sets of chamber data.

Altshuller and Bufalini^{9,20} have reviewed the various definitions of hydrocarbon reactivity and summarized results of numerous studies up to 1970. The criteria used for evaluating hydrocarbon reactivity include hydrocarbon consumption, the conversion of nitric oxide to nitrogen dioxide, ozone formation, aerosol formation, eye irritation and plant damage. It is generally agreed that the criteria most suitable with respect to photochemical oxidant control strategies are ozone dosage or maximum ozone concentration.³⁰ However, establishing a definitive hydrocarbon reactivity scale to be applied specifically to the control of ozone formation requires an extensive and lengthy experimental program in which the ozone-forming capability of each individual hydrocarbon is determined under simulated atmospheric conditions, including long-term irradiation (i.e., 10-12 hrs).

An alternative, and perhaps supplementary, basis for assessing hydrocarbon reactivity, which appears to have considerable utility and a valid experimental foundation, is the formulation of a reactivity scale based on the rate of disappearance of hydrocarbons due to their reaction with the hydroxyl radical, the key intermediate species in photochemical air pollution.

Results and Discussion

It is only comparatively recently that the critical role of OH in photochemical smog formation has been generally $\operatorname{recognized}^{40-44}$ and that appreciable rate constant data have become available for the reaction of OH with several classes of hydrocarbons. The importance of OH as a reactive intermediate relative to species such as 0_3 , $0(^3P)$, and $H0_2$ has been shown previously $^{43-46}$ through computer modeling of smog chamber data. For example, Niki, Daby, and Weinstock 43 showed that the reactivity of a number of hydrocarbons, as measured by the rate of conversion of NO to $N0_2$, correlated significantly better with OH rate constants than with either $0(^3P)$ or 0_3 rate constants.

The utility of a large environmental chamber in obtaining relative rate constants with an accuracy of $\pm 20\%$ for the reaction of the hydroxyl radical with a variety of hydrocarbons has been demonstrated in a number of recent studies both in this $^{45-48}$ and other laboratories. To date we have measured relative rates for the reaction of OH with some 35 organic compounds. The

detailed kinetic data derived from these investigations have been reported elsewhere. $^{45-48}$ In these studies we determined the relative rates of disappearance of selected alkanes, alkenes and aromatic hydrocarbons under simulated atmospheric conditions of temperature, pressure, concentrations, light intensity and other trace contaminants (NO $_{\rm x}$, CO, hydrocarbons, water). These relative rate constants were placed on an absolute basis using the published rate constants for OH + n-butane or isobutene. The assumption that OH was responsible for the hydrocarbon disappearance under the experimental conditions employed was subsequently supported by the very good agreement between OH rate constants determined for the individual compounds using flash photolysis-resonance fluorescence techniques 50,51 and those obtained in our initial chamber experiments. 45,46

The importance of the chamber method for the purposes of formulating a reactivity scale is that it permits the simultaneous determination of valid rate constants for reactions of OH with a large number and wide variety of atmospherically important hydrocarbons. This substantially expands the number of compounds which can be incorporated, now and in the near future, in the resulting reactivity scale.

Use of OH Rate Constants as a Reactivity Index

From the successful correlation of OH rate constants with the rates of hydrocarbon disappearance observed in chamber simulations at the SAPRC45-48 and Ford⁴⁹ laboratories we conclude that, to a good approximation, this correlation can be extrapolated to the atmosphere (a) for alkenes in ambient air parcels during the early morning hours when ozone levels are generally quite low (≤ 0.05 ppm), and (b) for alkanes and aromatics at essentially all times and locations. The latter assumption, namely that an OH rate constant is a good "reactivity index" for alkanes and aromatics throughout an irradiation day (or multiple irradiation days) rests upon the fact that the rates of reaction of these classes of hydrocarbons with species such as ozone, $O(^{3}P)$ atoms and the hydroperoxyl radical are several orders of magnitude slower than with $0H.^{8,52-54}$ For example, even at the highest ozone concentrations experienced in ambient atmospheres, 03 will not contribute significantly to the photooxidation of alkanes and aromatics. This is in contrast to the case for alkenes which, although the rate constants for reaction of 0_3 with alkenes are not particularly large, 55-57 react rapidly with ozone at the average concentrations commonly encountered in polluted ambient air (~0.1-0.2 ppm).

Proposed Reactivity Scale

Under the assumption that hydrocarbon depletion is due solely to attack by OH (with the qualification noted for alkenes), we propose a five-class reactivity scale based on hydrocarbon disappearance rates due to reaction with OH. The ranges of reactivities for the five proposed classes each span an order of magnitude in reactivity relative to methane and are shown in Table I. Although a scale based on OH rate constants can be divided into an arbitrary number of classes, we have found it convenient and useful (particularly for purposes of

comparison with other scales) to employ the order of magnitude divisions which lead to a five-class scale.

The hydrocarbon half-lives (defined as $t_{1/2} = 0.693/k[OH]$) corresponding to each class are also shown in Table I. These half-lives were calculated assuming depletion of the hydrocarbon solely due to reaction with the hydroxyl radical, and assuming an OH radical concentration in polluted atmospheres of 10^7 radicals cm⁻³, a reasonable value on the basis of both model calculations 58 and recent atmospheric measurements. 59-61

Table II shows the compounds, for which OH rate constants have been found or calculated, distributed among the five classes of our proposed reactivity scale in the order of increasing rates of reaction within each class. Employing OH rate constants obtained from hydrocarbon disappearance rates measured in photooxidation studies 62 , 63 as well as those from elementary rate determinations and our chamber studies, has permitted tabulation of OH rate constant data for 80 hydrocarbons. These 80 hydrocarbons are incorporated in Table II.

For interest, carbon monoxide although not a hydrocarbon, is included in Table II, since it is present in polluted urban atmospheres. Although CO is generally regarded as being "unreactive" in ambient air, in our scale it appears in Class II, which also includes ethane and acetylene.

In our current compilation of compounds, methane is the only compound listed which appears in Class I, although the recent work of Chameides and Stedman has shown that even methane will react given sufficient time. 64 Most of the straight chain alkenes appear in Class IV with the substituted alkenes occurring in the upper half of Class IV and in Class V. The alcohols fall into Class III while the monoterpene hydrocarbons are highly reactive and most of them appear in Class V with $\alpha-$ and $\beta-$ pinene occurring in the upper half of Class IV. The reactivity classification shown in Table II is similar to an earlier one we have formulated, 65 but many more compounds have now been included.

Comparison with Other Scales

The ranking of reactivities for the aromatic hydrocarbons in our scale is essentially the same as that obtained by Altshuller et al.4 and by Kopczynski. 7,66 Although our proposed scale is based solely on hydrocarbon disappearance rates, Altshuller and Bufalini on have shown that this measure of reactivity is very similar to the one based on nitric oxide oxidation rates. They showed that the ranking of reactivities of hydrocarbons from the nitric oxide photooxidation studies of Altshuller and Cohen and Glasson and Tuesday was essentially the same as that obtained from the studies of hydrocarbon consumption carried out by Schuck and Doyle, Stephens and Scott, and Tuesday.

As indicated above, Rule 66 formulated by the LAAPCD in 1966 represented the first hydrocarbon control measure based on photochemical reactivity. Although this and similar regulations have been effective, results from recent

studies $^{37-39}$ indicate that they give insufficient recognition to the ozone-forming potential of slow reactors, such as <u>n</u>-butane and propane under long-term irradiation conditions. Consequently, it is now realized that measures more stringent than Rule 66 are necessary to achieve reductions in ozone formation to levels approaching those mandated by the U. S. Clean Air Act Amendments of 1970.

Recognition of such deficiencies in current hydrocarbon control regulations has led to re-examination of present hydrocarbon reactivity classifications. The focus of these re-evaluations has been the five-class reactivity scale (see Table III) proposed by B. Dimitriades at the EPA Solvent Reactivity Conference in 1974.²⁵ Significant changes have been suggested for this reactivity classification by the California ARB,³⁰⁻³³ the LAAPCD,³⁴ the EPA,⁶⁷ and by industry. The EPA is currently examining this question and since no final conclusions have been reached at this time, we will restrict comparison of our proposed scale to the scale proposed in 1974 by Dimitriades of the EPA. In addition, we will discuss our proposed scale in the context of the three-class system recently approved³² by the ARB for application to hydrocarbon pollutant inventories and for planning future control strategies.

Briefly, the EPA has proposed, on the basis of previous experimental studies, that methane, ethane, acetylene, propane, and benzene are essentially non-reactive for typical urban ambient hydrocarbon-NO $_{\rm X}$ ratios 25 and these compounds are placed in Class I on their scale. Three other classes have been proposed for mobile source hydrocarbon emissions 68 —Class III (C $_4$ and higher alkanes), Class IV (aromatics less benzene) and Class V (alkenes). When stationary source hydrocarbons, including solvents (Class II), are added to the list, five classes are suggested as shown in Table III.

The reactivity classification proposed here (Tables I, II) can be compared with that suggested by the EPA (Table III). It is evident that several significant differences emerge:

- (1) The C_1 - C_3 alkanes are given equal weighting in the EPA scale and all are designated unreactive, while our scale clearly differentiates between the three compounds methane, ethane, and propane in Classes I, II, and III, respectively.
- (2) According to our proposed classification, benzene and \underline{n} -butane are of similar reactivity, while the EPA scale places them in Class I and III, respectively.
- (3) All the alkenes are placed in Class V of the EPA scale, while our proposed scale shows a differentiation in reactivity from ethene in Class III to 2,3-dimethy1-2-butene in Class V.
- (4) Our scale gives recognition to the high reactivity of natural hydrocarbons such as the pinenes and d-limonene, placing these in Class IV and V, respectively. The present published EPA scale does not give a classification for natural hydrocarbons, although they could be loosely categorized as substituted alkenes in Class V.

In addition to noting these differences, some similarities exist between the two scales. For example, our scale shows that 1,3-butadiene is highly reactive which is consistent with previous studies indicating it to be a facile precursor of eye irritants 20 and highly effective in producing oxidant during irradiation of HC-NO $_{\rm X}$ mixtures. 1 Both our scale and the EPA's show methanol to be relatively unreactive, with a greater reactivity exhibited by the higher alcohols, although our scale predicts a lower overall reactivity than that of the EPA.

The three-class system recently approved by the ARB is shown in Table IV and is similar to one being considered by the EPA. 30 According to the ARB, 32

"Class I would include low reactivity organic compounds yielding little, if any, ozone under urban conditions. Class II would consist of moderately reactive organic compounds which give an intermediate yield of ozone within the first day of solar irradiation. Class III would be limited to highly reactive organic compounds which give very high yields of ozone within a few hours of irradiation."

In general, the three-class ARB scale is in line with the scale presented here, based on OH rate constants, with only minor exceptions. For example, the ARB scale shows the primary and secondary C_{2+} alcohols to be highly reactive in Class III, while our scale shows them to be of moderate reactivity.

Finally, we wish to note two limitations of the reactivity scale proposed here. One limitation of our scale is that it is not strictly applicable to compounds which undergo significant photodissociation in the atmosphere, and aldehydes have been omitted for this reason. In such cases, the compound will be more reactive than predicted from a scale based on hydrocarbon depletion due solely to reaction with OH. A second limitation in the application of our scale concerns the inherent problem arising from uncertainties in the identity and fates of subsequent products.³³

Conclusion ·

Our proposed reactivity scale based on the depletion of hydrocarbons by reaction with the OH radical has utility in assessing hydrocarbon chemical behavior in polluted ambient air. Since only those organic compounds which participate in atmospheric reactions are of consequence in the chemical transformations in ambient air, their relative reactivity towards OH is a useful and directly measurable index of their potential importance in the production of secondary pollutants.

One advantage of the proposed scale is that, because it is based on the individual rate constants for hydrocarbon reaction with OH, any degree of gradation in reactivity may be used to formulate any desired number of classes—from relatively few to a large number of classes or even an ordered ranking of compounds. A second strength of the present scale is that it can be readily extended to include additional organic compounds once their rate of reaction

with OH is known. Finally, the proposed scale gives adequate weight to alkanes and a number of aromatic hydrocarbons which require a significant period of time to react but can contribute substantially to ozone formation during longer irradiation periods, e.g., during their transport downwind from urban centers—a phenomenon of increasing concern to air pollution control agencies.

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Table I. Reactivity Scale for Hydrocarbons Based on Rate of Disappearance of the Hydrocarbon due to Reaction with the Hydroxyl Radical.

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Class	Half-life ^a (days)	Reactivity Relative to Methane (= 1)
Ţ	≥ 10	≤ 10
II	1 - 10	10 - 100
III	0.1 - 1	100 - 1000
IA	0.01 - 0.1	1000 - 10,000
V	≤ 0.01	≥ 10,000

^a $t_{1/2} = 0.693/k_{OH}[OH]$. [OH] is assumed to be 10^7 radicals cm⁻³.

Proposed Reactivity Classification of Hydrocarbons and CO Based on Reaction with the Hydroxyl Radical Table II.

CLASS I	CLASS II	CLASS III	CLASS IV	CLASS V
(\$4.8×10 ⁷) ^a	$(4.8 \times 10^{7} - 4.8 \times 10^{8})^{a}$	$(4.8 \times 10^8 - 4.8 \times 10^9)^a$	$(4.8 \times 10^9 - 4.8 \times 10^{10})^a$	(>4.8×10 ¹⁰) ^a
Methane	Methano1	Neopentane	n-Octane	2-Methyl-2-butene
	Carbon monoxide	Cyclobutane	Diethyl ether	3-Carene
	Acetylene	2,2,3,3-Tetramethylbutane	p-Xylene	2,3-Dimethyl-2-butene
	Ethane	Benzene	p-Ethyltoluene	8-Phellandrene
		Ethyl acetate	o-Ethyltoluene	Carvomenthene
		Isobutane	o-Xylene	d-Limonene
		Propane	p-Cymene	Dihydromyrcene
		Diethyl ketone	Methyl isobutyl ketone	Myrcene
		Isopropyl acetate	Di-n-propyl ether	cis-Ocimene
		n-Butane	m-Ethyltoluene	
		n-Butyl acetate	m-Xylene	
		Ethanol	1,2,3-Trimethylbenzene	
		Methylethyl ketone	Propene	
		Isopentane	1-Butene	
		1-Propanol	3,3-Dimethyl-1-butene	
		2,2,4-Trimethylbutane	1-Pentene	
		2,3-Dimethylbutane	1-Hexene	
		2,2,3-Trimethylbutane	1,2,4-Trimethylbenzene	
		Tetrahydrofuran	Isobutene	
٠		2-Methylpentane	1,3,5-Trimethylbenzene	
		Toluene	cis-2-Butene	
		Cyclopentane	Difsobutyl ketone	
		n-Propylbenzene	2-Methyl-1-butene	
		Isopropylbenzene	α-Pinene	
		Ethene	Cyclohexene	
		n-Hexane	cis-2-Pentene	
		Cyclohexane	trans-2-Butene	
		n-Pentane	8-Pinene	
	٠,	p-Menthane	1,3-Butadiene	
		1-Butanol	Isoprene	
		Isopropyl alcohol		
		4-Methyl-2-pentanol		
		3-Methylpentane		
		Ethylbenzene		

Range of values (in liter mole sec 1) for the rate constant for reaction of the OH radical with the listed compounds.

Proposed EPA Reactivity Classification of Organics (from reference 25, 1974) Table III.

CLASS I (Nonreactive)	CLASS II (Reactive)	CLASS III (Reactive)	CLASS IV (Reactive)	CLASS V (Reactive)	
C ₁ -C ₃ paraffins	Mono-tertiary- alkyl benzenes	C_{4+} paraffins	Primary & Secondary alkyl benzenes	Aliphatic olefins	
Acetylene Benzene	Cyclic ketones	Cycloparaffins Styrene	Dialkyl benzenes	α-Methyl styrene Aliphatic aldehydes	
Benzaldehyde Acetone Methanol Tertiary-alkyl alcohols Phenyl acetate Methyl benzoate Ethyl amines Dimethyl formamide Perhalogenated	Tertiary-alkyl acetates 2-nitropropane	n-Alkyl ketones Primary & Secondary alkyl acetates N-methyl pyrrolidone N,N-dimethyl acetamide Partially halogenated paraffins	Branched alkyl ketones Primary & Secondary alkyl alcohols Cellosolve acetate Partially halogenated olefins	Tri- & tetra-alkyl benzenes Unsaturated ketones Diacetone alcohol Ethers Cellosolves	
REACTIVITY RATING: 1.0	3.5	, , ,	7.6	14.3	

Table IV. California Air Resources Board (ARB) Reactivity Classification of Organic Compounds 32

Class I (Low Reactivity	Class II (Moderate Reactivity)	Class III (High Reactivity)
C ₁ -C ₂ Paraffins	Mono-tert-alkyl-benzenes	All other aromatic hydro- carbons
Acetylene Benzene	Cyclic Ketones Alkyl acetates	All Olefinic hydrocarbons (including partially halo-
Benzaldehyde Acetone	2-Nitropropane C ₃₊ Paraffins	genated) Aliphatic aldehydes
Methanol Tert-alkyl alcohols	Cycloparaffins n-alkyl Ketones	Branched alkyl Ketones Cellosolve acetate
Phenyl acetate	N-Methyl pyrrolidone	Unsaturated Ketones
Methyl benzoate Ethyl Amines	N,N-dimethyl acetamide Alkyl Phenols*	Primary & Secondary C ₂₊ alcohols Diacetone alcohol
Dimethyl formamide Perhalogenated Hydrocarbons	Methyl phthalates**	Ethers Cellosolves
Partially halogenated paraffins		Glycols* C ₂₊ Alkyl phthalates**
Phthalic Anhydride** Phthalic Acids**		Other Esters** Alcohol Amines**
Acetonitrile* Acetic Acid		C ₃₊ Organic acids + di acid*
Aromatic Amines Hydroxyl Amines		C ₃₊ di acid anhydrides** Formin** (Hexa methylene-tetramine)
Naphthalene* Chlorobenzenes*		Terpenic hydrocarbons Olefin oxides**
Nitrobenzenes* Phenol*		

^{*}Reactivity data are either non-existent or inconclusive, but conclusive data from similar compounds are available; therefore, rating is uncertain but reasonable.

^{**}Reactivity data are uncertain.

RELATIVE RATE CONSTANTS FOR THE REACTIONS OF OH RADICALS WITH ISOPROPYL ALCOHOL, DIETHYL AND DI-n-PROPYL ETHER AT 305 \pm 2 K

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Relative rate constants have been obtained for the reaction of the hydroxyl radical (OH) with isopropyl alcohol and diethyl and di-n-propyl ether in environmental chamber photooxidation studies employing hydrocarbon- NO_X mixtures in air at 1 atmosphere and 305 ± 2 K. These results were obtained from measurements of the relative rates of disappearance of these compounds on the previously validated basis that OH radicals are dominantly responsible for their disappearance in the initial stages of reaction under the experimental conditions employed. Absolute rate constants, obtained by using the published rate constant for OH + isobutene of $3.05 \times 10^{10} \, \Omega$ mole⁻¹ s⁻¹ are $(k \times 10^{-9} \, \Omega$ mole⁻¹ s⁻¹): isopropyl alcohol, 4.3 ± 1.3 ; diethyl ether, 5.6 ± 1.1 ; and di-n-propyl ether, 10.4 ± 2.1 . No previous determinations of these rate constants have been reported.

1. Introduction

The hydroxyl radical plays a fundamental role in chemical transformations in photochemical air pollution [1-7]. With the realization of the importance of OH has come an extensive experimental effort to determine rate constants for the reaction of OH with a large number of organic compounds. These studies have been documented in recent reviews [7] and in a critical compilation [8].

To date, however, comparatively few data have been obtained for the gas phase reactions of OH with oxygenated hydrocarbons [9–11]. In this work, rate constants are reported for the reaction of OH with three ingredients of commercial solvents [12,13] — isopropyl alcohol and diethyl and di-n-propyl ether. Such data are of fundamental importance in assessing the role of these oxygenated hydrocarbons in atmospheric chemistry, particularly since, as controls on automobiles reduce the contribution of hydrocarbons from mobile sources, emissions of such oxygenates from stationary sources become increasingly of greater concern.

2. Experimental

The technique used to determine relative OH rate constants in this study has been previously employed to obtain kinetic data for reactions of OH with alkanes [14,15], alkenes [11,15], ketones [11], aromatics [14,15], and halogenated [11,16] and natural hydrocarbons [11]. Briefly, irradiations of the hydrocarbon-NO_x—air system were carried out in a Pyrex chamber of approximately 6400-liter volume at a light intensity, measured as the rate of NO₂ photolysis in nitrogen (k_1) , of 0.4 min⁻¹. All gaseous reactants were injected into pure matrix air [17] in the chamber using 100-ml precision bore syringes. Liquid reactants were injected with micropipettes. During irradiation, the chamber temperature was maintained at 305 ± 2 K.

The alcohol and ether concentrations were monitored with gas chromatography (FID), using a 5-ft. \times 1/8-in. stainless steel column packed with Poropak Q (80–100 mesh), operated at 393 and 423 K, respectively. Ozone was monitored by means of ultraviolet absorption; CO, by gas chromatography; and NO-NO₂-NO_x, by the chemiluminescent reaction of NO with ozone.

The initial concentrations of reactant were isopropyl alcohol, 60 ppb (1 ppb in air $\equiv 4.0 \times 10^{-11}$ mole liter $^{-1}$ at 305 K and 1 atmosphere); diethyl ether, 20 ppb; and di-n-propyl ether, 55 ppb. In addition to these compounds, traces of several alkanes, alkenes and oxygenates were present [11,15]. Initial concentrations in these experiments were 800-1500 ppbC of total non-methane hydrocarbons, 0.60 ppm of NO_x (with an NO_2/NO_x ratio of 0.03–0.08), 6 ppm of CO, and 3000 ppb of methane, together with warer vapor at 50% relative humidity. Replicate 3-hour irradiations were carried out with continuous analysis of inorganic species, analysis of hydrocarbons every 15 minutes, and analysis of isopropyl alcohol and the ethers every 30 minutes.

All data were corrected for losses due to sampling from the chamber by subtraction of the average dilution rate (1.2–1.6% per hour) from the observed hydrocarbon disappearance rate. The HC/NO_x and NO/NO_2 ratios were chosen to delay the formation of ozone, and ozone was not detected during the irradiation period [11,14].

As discussed in detail previously [11,15], the major sources of OH in our experimental system are probably the photolysis of HONO and the reaction of HO₂ with NO [5,6,18,19];

$$NO + NO_2 + H_2O \rightleftharpoons 2 \text{ HONO}, \tag{1}$$

$$HO_2 + NO_2 \rightarrow HONO + O_2$$
, (2)

$$HONO + hv(290-410 \text{ nm}) \rightarrow OH + NO$$
, (3)

$$HO_2 + NO \rightarrow OH + NO_2$$
. (4)

The first reaction is thought to occur relatively slowly homogeneously [20,21], but its rate is probably significantly faster when the reaction is catalyzed by surfaces. Thus, nitrous acid has been observed in a chamber study of simulated atmospheres carried out in our laboratory [22], while direct evidence for formation of OH radicals in an environmental chamber has been provided recently by Niki, Weinstock and co-workers [23,24].

The concentration of OH radicals present during these irradiation experiments was calculated to range from 1.4 to 3.5×10^6 radicals cm⁻³, depending upon the conditions of the specific experiment. The calculations employed the observed rates of isobutene dis-

appearance (corrected for dilution) and the previously determined rate constant for OH + isobutene [25]. These concentrations are the same order as those calculated [18,26,27] and observed directly [23,24,28, 29] by other workers.

3. Results and discussion

Typical rates of disappearance observed during the irradiations of isopropyl alcohol and of the two ethers are shown in figs. 1 and 2, respectively. Isobutene was used as the reference compound and is included in the figures. From these pseudo-first-order rates of disappearance of the hydrocarbons, rate constants relative to that of isobutene were obtained for the reaction of the PH radical with isopropyl alcohol and diethyl and di-n-propyl ether. These were placed on an absolute basis, using a value of $3.05 \times 10^{10} \, \mathrm{g}$ mole⁻¹ s⁻¹ for the reaction of OH with isobutene [25]. These results are presented in table 1.

There are no rate constants currently available for the reaction of OH radicals with ethers. Assuming that hydrogen abstraction is the major reaction pathway, one would expect these rate constants to be larger than

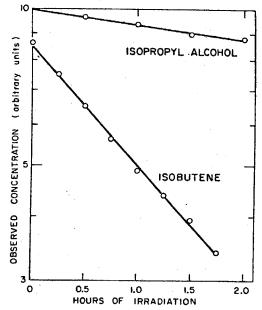


Fig. 1. Concentrations of isopropyl alcohol and isobutene (plotted on a logarithmic scale) during photolysis of $HC-NO_X$ mixture in air at 305 ± 2 K and 1 atm.

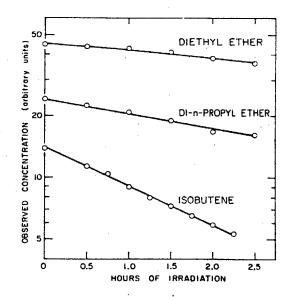


Fig. 2. Concentrations of diethyl and di-n-propyl ether and isobutene (plotted on a logarithmic scale) during photolysis of HC-NO $_{\rm x}$ mixture in air at 305 \pm 2 K and 1 atm.

those for the corresponding alkane, since the C-H bond strengths in the ethers are at least several kilocalories weaker [30]. Thus, our rate constants (at 305 K) for diethyl and di-n-propyl ethers of 5.6 and $10.4 \times 10^9 \ \text{g}$ mole⁻¹ s⁻¹, respectively, compare with values for the corresponding alkanes, n-butane and n-hexane (at 298 K) of 1.6 and $2.9 \times 10^9 \ \text{g}$ mole⁻¹ s⁻¹, respectively, calculated from the formula of Greiner [31].

Two recent measurements of the rate constants for the gas phase reaction of OH radicals with alcohols

have been reported. Osif et al. [9] obtained a value of 5.3×10^7 ℓ mole⁻¹ s⁻¹ for OH + methanol using a value of 8.4×10^7 ℓ mole⁻¹ s⁻¹ for OH reaction with CO [8]. Recently, Campbell et al. [10] have carried out studies of the reaction of OH with a series of alcohols—methanol, ethanol, 1-propanol and 1-butanol. Our value for OH + isopropyl alcohol of $(4.3 \pm 1.3) \times 10^9$ ℓ mole⁻¹ s⁻¹ at 305 K is consistent with the value of $(2.3 \pm 0.2) \times 10^9$ ℓ mole⁻¹ s⁻¹ reported for 1-propanol by Campbell et al. [10] at 292 K.

Although, as mentioned, no literature data are available for the reaction of OH with ethers, it is interesting to examine the data for solvent photooxidations obtained by Laity et al. [32] in chamber studies. These workers irradiated separate solvent-NO_x-air mixtures in a stainless steel chamber at 305 K and reported the maximum rate of hydrocarbon disappearance observed in these experiments relative to toluene. If this disappearance is assumed to be predominantly due to attack by OH, then absolute rate constants may be derived from these data, using a value of 3.6 $\times 10^9$ l mole⁻¹ s⁻¹ for the reaction of OH + toluene [33,34]. Values for OH + isopropyl alcohol and OH + diethyl ether are 3.1 \times 10⁹ and 5.4 \times 10⁹ ℓ mole⁻¹ s⁻¹, respectively, compared to our results of 4.3 and 5.6 × 109 2 mole⁻¹ s⁻¹. Considering the differences in experimental methods and apparatus, as well as the uncertainties involved in such an interpretation of the data of Laity et al. [32], the agreement obtained for isopropyl alcohol and diethyl ether is quite satisfactory. Similar treatment of their chamber data for other compounds for which the OH rate constants are known yields results [35] in fair agreement with literature values.

Table 1
Relative and absolute rate constants for the reaction of OH with selected hydrocarbons

Compound	Relative rate of	$k(2 \text{ mole}^{-1} \text{ s}^{-1} \times 10^{-9})$				
	disappearance	this work a)	literature			
isobutene	1	30.5				
isopropyl alcohol	0.14	4.3	3.1 b)			
diethyl ether	0.185	5.6	5.4 b)			
di-n-propyl ether	0.34	10.4				

a) Using a literature value of $3.05 \times 10^{10} \ \text{g mole}^{-1} \ \text{s}^{-1}$ for OH + isobutene [25].

b) Using the data of Laity et al. [32] and attributing the HC loss solely to reaction with OH; results placed on an absolute basis using a value of 3.6 × 10⁹ 2 mole⁻¹ s⁻¹ for OH + toluene (see text).

The atmospheric half lives, $t_{1/2} = 0.693/k_{\rm OH}$ +RH \times [OH], for isopropyl alcohol and diethyl and di-n-propyl ether are calculated to be 5.4, 4.1 and 2.2 hours, respectively, using an ambient OH concentration of 5×10^6 radicals cm⁻³ [18,23,24,26–29] and our rate constants. Thus, these compounds react with OH at rates similar to ethene, $C_6 - C_7$ alkanes, and mono-alkyl substituted benzenes [36]. The relative importance of alcohols, ethers and other oxygenated hydrocarbons in photochemical smog formation are discussed in detail elsewhere [35–37].

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RELATIVE RATE CONSTANTS FOR THE REACTION OF OH RADICALS WITH SELECTED C_6 AND C_7 ALKANES AND ALKENES AT 305 \pm 2 K

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Measurements of the rates of disappearance of three alkenes and two alkanes relative to isobutene in environmental chamber photooxidation studies employing hydrocarbon— NO_X mixtures in air at 1 atmosphere have been used to obtain relative rate constants for the reaction of these compounds with the hydroxyl radical. Absolute rate constants at 305 \pm 2 K obtained using a published rate constant for OH + isobutene of $3.05 \times 10^{10} \, \Omega$ mole⁻¹ s⁻¹ are $(k \times 10^{-9} \, \Omega)$ mole⁻¹ s⁻¹): cyclohexene, 47 \pm 9; 1-methylcyclohexene, 58 \pm 12; 1-heptene, 22 \pm 5; 2, 3-dimethylbutane, 3.1 \pm 0.5; 2, 2, 3-trimethylbutane, 2.3 \pm 0.5. No previous determinations of OH rate constants have been reported for 1-heptene and 1-methylcyclohexene. For the remaining compounds these results are shown to be in good agreement with literature values reported for elementary, or relative rate constant determinations.

1. Introduction

Recently, we have reported rate constant determinations for the reaction of OH with alkanes [1, 2], alkenes [2, 3], aromatic hydrocarbons [1, 2], monoterpene hydrocarbons [3], halogenated hydrocarbons [3, 4], ketones [3], and ethers and isopropyl alcohol [5]. These rate constants were obtained by measuring the relative rates of disappearance of hydrocarbons in a hydrocarbon-NO, mixture in air at 1 atmosphere and at 305 ± 2 K. Absolute rate constants were obtained [1-3, 5] by using literature values for OH + nbutane and/or isobutene, at least one of which was employed as a reference compound in each study. A similar technique has recently been employed by Niki and co-workers [6]. Results obtained from these relative rate studies have uniformly been in very good agreement with literature values reported for elementary rate constant determinations [7].

Here we report rate constant data at 305 ± 2 K for the reaction of OH with 1-heptene, 1-methylcyclohexene, cyclohexene, and two substituted alkanes — 2, 3-dimethylbutane and 2, 2, 3-trimethylbutane. These long-chain alkanes and cyclic alkenes have been suggested to play a major role in the formation of the organic portion of aerosols found in polluted ambient air [8,9].

2. Experimental

The experimental technique used to determine relative OH rate constants in this study has been described in detail previously [1-3]. Briefly, irradiations of the hydrocarbon- NO_x -air system were carried out in a Pyrex chamber of approximately 6400-liter volume at a light intensity, measured as the rate of NO_2 photolysis in nitrogen (k_1) , of 0.4 min⁻¹. During irradiation, the chamber temperature was maintained at 305 ± 2 K.

The alkane and alkene concentrations were monitored with gas chromatography (FID), using a 5' \times 1/8" SS of Poropak Q (80-100 mesh) column and a 36' \times 1/8" SS column of 10% dimethylsulfolane on AW C-22 Firebrick (60-80 mesh) followed by 18" \times 1/8" SS column of 10% Carbowax 600, operated at 433 and 273 K, respectively. Ozone was monitored by means of ultraviolet absorption; CO by gas chromatography, and NO-NO₂-NO_x by the chemiluminescent reaction of NO with ozone.

The initial concentrations of reactants were 2, 3-dimethylbutane, 7 ppb (1 ppb in air $\equiv 4.0 \times 10^{-11}$ mole liter⁻¹ at 305 K and 1 atmosphere); 2, 2, 3-trimethylbutane, 14 ppb; cyclohexene, 10 ppb; 1 methylcyclohexene, 21 ppb, and 1-heptene, 14 ppb. In addition to these compounds, traces of several alkanes, alkenes, and oxygenates were present [2, 3]. Initial

concentrations in these experiments were 700–800 ppbC of total non-methane hydrocarbons, 0.61 ppm of NO_x (with an NO_2/NO_x ratio of 0.04–0.05), 6 ppm of CO, and 2900 ppb of methane, together with water vapor at 50% relative humidity. Replicate three-hour irradiations were carried out with continuous analysis of inorganic species and analysis of hydrocarbons every 30 minutes.

All data were corrected for losses due to sampling from the chamber by subtraction of the average dilution rate (1.6% per hour) from the observed hydrocarbon disappearance rate. The HC/NO_x and NO/NO_2 ratios were chosen to delay the formation of ozone, and ozone was not detected during the irradiation period [1,3].

As discussed in detail previously [2,3], the major sources of OH in our experimental system are probably the photolysis of HONO and the reaction of HO_2 with NO [10-13]:

$$NO + NO_2 + H_2O = 2 HONO,$$
 (1)

$$HONO + hv (290-410 \text{ nm}) \rightarrow OH + NO$$
, (2)

$$HO_2 + NO \rightarrow OH + NO_2$$
. (3)

The first reaction is thought to occur relatively slowly homogeneously [14–16], but its rate is probably significantly faster when the reaction is catalyzed by surfaces. Thus, nitrous acid has been observed in a chamber study of simulated atmospheres carried out in our laboratory [17], while direct evidence for formation of OH radicals in an environmental chamber has been provided recently by Niki, Weinstock and co-workers [6, 18, 19]. The reaction of HO₂ with NO₂ has also been proposed as a source

$$HO_2 + NO_2 \rightarrow HONO + O_2$$
 (4)

of nitrous acid [20,21], but recent results [22,23] suggest that peroxynitric acid is the major product of reaction (4).

$$HO_2 + NO_2 \rightarrow HO_2NO_2. \tag{5}$$

The peroxynitric acid may decompose back to HO_2 and NO_2 , or possibly give HONO, but this is currently uncertain [22, 23].

The concentration of OH radicals present during these irradiation experiments was calculated to range

from $(2.5-5.0) \times 10^6$ radicals cm⁻³ depending upon the conditions of the specific experiment. The calculations of OH concentrations employed the observed rates of isobutene disappearance (corrected for dilution) and the previously determined rate constant for OH + isobutene [24]. These concentrations are the same order as those calculated [12, 25, 26] and observed directly [18, 27, 28] by other workers.

3. Results and discussion

Isobutene was used as the reference compound in this series of experiments. From the pseudo-first-order rates of disappearance of the hydrocarbons, rate constants relative to that of isobutene were obtained for the reaction of the OH radical with 2, 3-dimethylbutane, 2, 2, 3-trimethylbutane, cyclohexene, 1-methylcyclohexene and 1-heptene. These were placed on an absolute basis using a value of $3.05 \times 10^{10} \ \text{g}$ mole⁻¹s⁻¹ for the reaction of OH with isobutene [24]. These results are presented in table 1, together with the available literature data.

Within the estimated 20% uncertainty in our rate constant values, the agreement among our data and the literature values is good. For example, our value of $(3.1 \pm 0.6) \times 10^9$ & mole⁻¹s⁻¹ for 2, 3-dimethylbutane agrees within experimental uncertainty with that of $(2.6 \pm 0.3) \times 10^9 \ \ell \ \text{mole}^{-1} \text{s}^{-1}$ recently determined in a separate study in this laboratory by Atkinson et al. [4]. This latter value was derived from the relative rates of disappearance of 2,3-dimethylbutane and ethane during a 216-hour irradiation in the Pyrex chamber. Both of these values are significantly lower than the value directly determined by Greiner [29] at 300 K of $(5.16 \pm 0.13) \times 10^9$. However, it is expected [28] that the rate constant for the reaction of OH radicals with 2, 3-dimethylbutane would be less than twice as fast as with isobutane on the basis of the numbers of primary and tertiary hydrogen atoms in these two alkanes. The absolute rate constant for the reaction of OH radicals with isobutane has been determined to be 1.5×10^9 ft mole⁻¹s⁻¹ at 304 K [29], and hence the OH rate constant for 2, 3-dimethylbutane is expected to be $\leq 3 \times 10^9 \, \ell \, \text{mole}^{-1} \, \text{s}^{-1}$ which is in agreement with both the determination of Atkinson et al. [4] and with the present work.

Similarly, our value of $(2.3 \pm 0.5) \times 10^9 \ \ell \ \text{mole}^{-1}$

Table 1
Pelative and absolute rate constants for the reaction of OH and O(³P) with selected hydrocarbons

•		$k(\ell \text{ mole}^{-1} \text{ s}^{-1}$	× 10 ⁻¹⁰)	•	
Compound	Deletine ma	kOII + compour			
Compound	Relative rate of disappearance	this work a)	literature	$k_{O(^3P)}$ + compound at 298 K	
isobutene	1	3.05		1.2 e)	
2, 3-dimethylbutane	0.10	0.31 ± 0.06	0.45 b), 0.26 ± 0.03 c)	0.012 e)	
2, 2, 3-trìmethylbutane	0.074	0.23 ± 0.05	0.29 b)	0.012	
1-pentene	-		$1.8 \pm 0.2 d$)	0.28 e)	
1-hexene	_	_	$1.9 \pm 0.2 d$	0.31 e)	
l-heptene	0.73	2.2 ± 0.5	=	0.51	
cyclohexene	1.53	4.7 ± 0.9	$3.8 \pm 0.4 \text{ d}$	1.3 e)	
1-methylcyclohexene	1.91	5.8 ± 1.2	_	$4.9 \pm 0.2 \text{f}$	

a) Using a literature value of $3.05 \times 10^{10} \, \Omega$ mole⁻¹ s⁻¹ for OH + isobutene [24].

b) Ref. [29], T = 298 K. c) Ref. [4], T = 305 K.

d) Ref. [16] using a literature value of $3.1 \times 10^{10} \, \ell$ mole⁻¹ s⁻¹ at 303 K for OH + cis-2-butene [24].

e) Ref. [32]. f) Ref. [31].

s⁻¹ for 2, 2, 3-trimethylbutane is in reasonable agreement with the value of $(2.9 \pm 0.1) \times 10^9$ k mole⁻¹ s⁻¹ obtained by Greiner at 303 K [29]. In addition, the decrease in rate constant in going from 2, 3-dimethylbutane to the larger molecule 2, 2, 3-trimethylbutane is consistent with a decrease from two to one in the number of tertiary hydrogen atoms [29]. These atoms are the most easily abstracted, since the C-H bond strength for tertiary hydrogens is 3 kcal mole⁻¹ and 6 kcal mole⁻¹ weaker than that for secondary and primary hydrogens, respectively [30].

Recently, Wu et al. [6] used a technique similar to the one employed here, namely, the photooxidation of hydrocarbons in the presence of NO_x in air at 1 atmosphere and 303 K. Under the assumption that OH was the principal species depleting the hydrocarbon, they obtained rate constants relative to cis-2-butene for several of the higher alkenes. Using a value of 3.1 \times 10¹⁰ ℓ mole⁻¹ s⁻¹ for OH + cis-2-butene at 303 K [24], one obtains a value of 3.8 \times 10¹⁰ mole⁻¹ s⁻¹ for cyclohexene at 303 K from the data of Wu et al. [6]. This value is in reasonable agreement with our value of $(4.7 \pm 0.9) \times 10^{10} \ell$ mole⁻¹ s⁻¹ at 305 K.

Substitution of a methyl group for one of the hydrogen atoms in cyclohexene increases the rate constant slightly, since we obtain a value of $(5.8 \pm 1.2) \times 10^{10} \, \ell \, \text{mole}^{-1} \, \text{s}^{-1}$ for 1-methylcyclohexene. This is expected by analogy with the similar

addition reaction of $O(^3P)$ atoms with cyclohexene and 1-methylcyclohexene (0.91 and 4.21 relative to $O(^3P)$ + cyclopentene) [31].

Table 1 shows a comparison of the reactivity of $O(^3P)$ atoms [31,32] as well as OH radicals towards the compounds studied here and other selected compounds. Since both $O(^3P)$ and OH are expected to primarily undergo addition to the alkenes, one would expect the same trend in going from 1-pentene to cyclohexene and this is, in fact, observed. In addition, the value of $1.8 \times 10^{10} \, \ell$ mole $^{-1} \, s^{-1}$ obtained for 1-hexene by Wu et al. [6] and our value of $2.2 \times 10^{10} \, \ell$ mole $^{-1} \, s^{-1}$ for 1-heptene, both obtained by similar methods, are consistent with the trend observed by Wu et al. [6] of an increase in rate constant with the larger molecular size of the alkene.

As mentioned above, the higher straight chain and cyclic alkenes are assumed to be important precursors of the organic content of ambient aerosols found in polluted air [9,10]. The rapid rate of reaction of OH with these species ensures that, in addition to O_3 —alkene reactions, OH attack will be an important reaction pathway in real and simulated atmospheres, possibly yielding multifunctional oxygenated species in the aerosol phase [9,33].

Assuming an ambient OH concentration of 5×10^6 radicals cm⁻³ [18, 27, 28], the atmospheric half-lives, $t_{1/2} = 0.693/k_{\rm OH+RH}$ [OH], based solely on reaction

with OH, are (in hours): 2,3-dimethylbutane, 7.5; 2,2,3-trimethylbutane, 10.0; cyclohexene, 0.49; 1-methylcyclohexene, 0.39; and 1-heptene, 1.0. In the case of the alkenes, the actual half-lives in the atmosphere are expected to be significantly less, since O₃ reacts with the alkenes at significant rates [9, 34].

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APPENDIX B

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Sundail form, Inc.	1930		33.2	2.0	C.299							
<b>ģ</b> (	1945		33.1	2.0	0.297		'					
<u>.</u> 2	2000		33.2	2.0	C.300							
. 📲 🔔	2015		33.4	2.0	C.310	*	•			4		
§C.	. 2030		33.5	2.0	0.296							
ğ	2045		33.7	2.0	0.307							
	2100		33.7	2.0	C.299							
<u>3</u> (.	2115		33.8	2.0	0.294							
C	2130		33.7	2.0	0.300			·				
	2145		33.8	2.0	0.295				,			
C	2200		33.7	2.0	0.296	•						
	2215		33.7	2.0	0.296.							
<u>~.</u>	2230		33.7	2.0	0.294							
C	2245		33.7	2.0	0.294							
	2300		33.7	2.0	C.291							
-	2315		33.7	2.0	0.237				•			
C	2330		33.7	2.0	0.283							
	2345		33 <u>.4</u>	2.0	0.291							
(			33.4	2.0	0.285							
<u> </u>	15	735.	33.4	2.0	0.238	•						
		**** NO C	ATA TAKEN		DATA	DISCARCE	3	? QUESTIONA	BLE DATA	Apparent species or cut reactions and other a receipting		
C												
,					•							
( ,												

	GLA	-216-3 SI				
		'6 JUL 28				
	PM WATER COMP.					
			*		•	
						The second secon
-	CLOCK	ELAPSEC	TS1	REL HUM		
	TIME T	INE (NIM)	(DEG C)	(3)	(844)	
						The state of the second control of the state
	30 45	750. 765.	33.9 34.6	2.0	C.287 C.278	
-	100	780.	35.0	2.0	C.250	Control of the contro
	115	795.	35.4	1.5	C.276	
	130	810.	35.4	1.5	C.281	
	145 200	625. 840.	35.4 35.4	1.5	C.277	
	215	855.	35.6	1.5	C.277	
_	230	870.	35.6	1.5	C - 281	
	245	885.	35.4	1.5	C-275	
	300	900. 915.	35.6	1.5	C.270	
	315 330	930•	35.4 35.6	1.5 1.5	C.269 C.271	THE REPORT OF THE RESIDENCE OF THE SECOND STATES AND ADDRESS OF TH
	345	945.	35.4	2.0	0.271	
_	400	960.	35.4	1.5	C.261	
	415	975.	35.4	2.0	C.250	
	430 445	990. 1005.	35.4 35.3	2.0	C.264	the state of the s
	500	1020.	35.4	2.0	C.260	
	515	1035.	35.3	2.0	C.250	
	530	1050.	35.3	2.0	0.254	
	545	1065.	35.4	2.0	0.250	
	600 615	1080.	35.1 35.0	2.0	0.252 C.249	
-	630	îiio.	35.0	2.0	0.248	The first three products are the second of t
	645	1125.	35.0	2.0	0.249	
	700	1140.	35.0	2.0	0.249	
	715 730	1155. 1170.	35.0 35.0	2.0	0.243 0.244	
	745	1185.	35.0	2.5	C.239	
	800	1200.	34.7	2.5	C.238	A HARMAN CO. THE PERSON OF THE
	815	1215.	34.7	2.5	0.238	
_	830	1230.	34.5	2.5	0.236	
	845 <b>9</b> 00	1245. 1260.	34.5 34.7	2.5	C.241 C.237	
		1275.	34.7	2.5		
-	930	1295.	34.7	2.5	0.236	A COMMENT OF THE STATE OF THE COMMENT OF THE COMMEN
	945	1305.	34.7	2.5	C.231	
	1000_	1370 •	34.7	2.• 5_	C.233	ON OFFICE AND ADDRESS OF THE PROPERTY OF THE P
	1015 1030	1335. 1350.	34.7 34.7	2.5 2.5	C.232 C.226	
	1045	1365.	34.7	2.5	0.225	
-	1100	1300.	34.9	2.5	C.227	Control to the first transfer of the control of the
	1115	1395.	34.9	2.5	C-226	
-	1130	1410		2.5.	C.216	THE COLUMN TWO IS NOT THE WARRANT TO THE WARRATT TO THE WARRANT TO THE WARRANT TO THE WARRANT TO THE WARRANT TO
	1145	1425.	34.7	2.5	C-215	

```
DATA FOR 216-LIGHT USELESS DUE TO FAULTY DACS CHANNEL
SOZ STRIP CHART DATA USED FOR THIS RUN
2.5 ML CF SOZ INJECTED HITH 90 ML OF NZ ON JULY 30 AT 1003
DASIBI 1212 ON CHAMBER AT ABOUT 1534 TO 1537 ON JULY 30 AND FROM 1201 TO
     1230 CN JULY 31
SAMPLING RATES (ML/MIN): TECO 43 - 1161; DASIBI 1212 - 600
                                  T$1
                                         REL HUM
                                                      SO<sub>2</sub>
 TIME TIME(MIN)
                      ( PPM )
                               (DEG C)
                                           (2)
                                                    ( PPM )
  1130
              -15.
                     ****
                                                    0.328
  1145
                0.
                     *****
                                 34.6
                                           22.0
                                                    0.321
  1200
               15.
                     *****
                                 35.1
                                            21.5
                                                    0.315
  1215
               30.
                     *****
                                 35.4
                                            19.5
                                                    C.310
  1230
                                 35.6
               45.
                     ***
                                            18.3
                                                    0.307
  1245
               60...
                     ****
                                  35.7
                                           17.0
                                                    0.305
  1300
               75.
                     *****
                                 36.0
                                            16.5
                                                    0.301
  1315
               90.
                     ****
                                 36.0
                                            15.5
                                                    0.296
  1330
              1C5.
                     *****
                                 36.1
                                           14.5
                                                    0.292
  1345
              120.
                     *****
                                  36.4
                                           13.0
                                                    C.290
  1400
              135.
                     ****
                                 36.6
                                           11.0
                                                    0.286
  1415
                                 36.6
              150. ..
                     *****
                                           11.5
                                                    0.282
  1430
              165.
                     ****
                                 36.5
                                                    0.279
  1445
                     ****
              180.
                                 36.5
                                            11.0
                                                    0.276
             195.
  1500
                     *****
                                 36.2
  1515
              210.
                     *****
                                 36.1
                                           13.0
                                                    0.269
  1530
              225.
                      0.519
                                 36.0
                                            14.0
                                                    0.265
             240.
255.
  1545
                     ****
                                 35.8
                                           15.0
                                                    0.262
  1600
                     *****
                                 35.7
                                           15.5
                                                    C-260
  1615
              270.
                     *****
                                 35.7
                                            16.0
                                                    0.255
  1630
             285.
                     *****
                                  35.7
                                            16.5
                                                    0.253
  1645
              300.
                                 35.7
                                           17.0
                                                    0.250
  1700
              315.
                                 35.7
                                            17.0
                                                    0.25C
              330.
                                 35.7
                                            18.0
                                                    0.247
              345.
                                            19.0
                                                    0.245
  1745
              360.
                     *****
                                 35.6
                                           20.0
                                                    0.242
  1800
              375.
                     *****
                                  35.4
                                           21.0
                                                    0.240
             390.
  1815
                     *****
                                 35.4
                                           22.5
                                                    0.237
  1830
              4 C5.
                     ****
                                 35.7
                                           21.5
                                                    0.236
  1845
              420.
                     *****
                                 36.1
                                           19.0
                                                    0.235
  1900
             435.
                     *****
                                 36.4
                                            17.0
                                                    0.233
  1915
              450.
                     ****
                                 36.5
                                            16.0
  1930
             465.
                     *****
                                 36.6
                                           15.5
                                                    0.227
             480.
  1945
                     *****
                                 36.6
                                           14.5
                     ****
  2000
             495.
                                 36.6
                                           15.0
                                                    0.222
  2015
             510.
                     *****
                                 36.6
                                           15.0
                                                    0.220
                     ****
  2030
             525.
                                 36.6
                                           15.5
  2045
             540.
                     *****
                                 36.6
                                           15.5
                                                    0.216
             555.
  2100
                     ****
                                                    0.213
                                 36.6
                                           15.5
             570.
  2115
                                 36.5
                                           16.5
                                                    G.211
  2130
             585.
                                 36.5
                                           17.0
                                                    0.210
  2145
              600.
                                 36.5
                                            17.5
                                                    0.208
  2200
             615.
                                 36.4
                                           18.0
                                                    0.206
  2215
             630.
                                 36.4
                                           18.0
                                                    0.204
  2230
             645.
                                 36..2
                                           19.0
                                                    0.203
             660.
                                 36.4
                                           19.5
                                                    C-200
  2300
2315
2330
             675.
                                 36.2
                                           20.0
                                                    0.196
             690.
                     *****
                                 36.2
                                           20.5
                                                    0.195
             705.
                                 36.1
                                                    0.193
  2345
             720.
                                 36.1
```

AGC-217-1 SO2 LIGHT DRY. GLASS CHAMBER

NO DATA TAKEN

CONTINUATION OF AGC-216 LIGHT; LIGHTS ON JUL 29 AT 1000: INTENSITY 100%

1976 JUL 30

? QUESTIONABLE DATA

DATA DISCARDED

AGC-217-2 SO2 LIGHT DRY GLASS CHAMBER 1976 JUL 31

	TIME TIME	ELAPSED TIME(MIN)	(PPM)	IDEG C)	REL HUM.	SC2 (PPM)	
	ő	735.	****	36.0	22.C	0.188	
	15	750.	****	36.0	22.0	C.185	
	30	765	*****		22.0		
	45	780.	****	35.8	22.0	0.181	
	100	795.	****	35.8	22.5	0.180	
	115	810	*****	35.8			
	130	825.	****	35.7	22.5	0.175	
	145	840.	****	35.7		0.172	
	200	855.		35.7		G.171	
	215 230	870. 885.	****	35.6	22.5	0.169	
	245	900		35.6 35.6	23.0	0.168	
	300	915.	*****	35.6	23.0		
	315	930.	*****	35.6	23.0 23.0	0.163 C.160	
	330	945.	*****	35.6			
	345	960.	*****	35.6	23.0	0.158	
	4C0	975.	*****	35.4	23.0	0.156	
_	415	990.	****	35.6		0.154	
	430	1005.	*****	35.6	23.5	0.152	
	445	1020.	****	35.4	23.5	0.150	
	500_	1035.	*****	35.4	23.5		
	515	1050.	*****	35.4	23.5	G.147	
	530		*****	35.4	23.5	0.145	
	545	1080•	***	35.4	23.5	0.144	
	600	1095.	****	35.4	23.5	C.142	
	615	1110.	****	35.4	23.5	0.140	
	630		*****	35.4	24.0		
	645 700	1140. 1155.	*****	35.4	24.0	0.137	
	715	1170.	*****	35.4 35.4	24.0	0.135	
	730	1185.	*****	35.4	24.0 24.0	0.134	-4-
	745	1200.	*****	35.4	24.0	0.133	
	800	1215.	*****	35.3	24.C		
	815	1230.	****	35.4	24.0	0.128	٠,,
	830	1245.	*****	35.4	24.5	0.127	
	845	1260.	* * * * *	35.4	24.5	0.126	
	900	1275.	****	35.4	24.5	0.124	
	915	1290.	****	35.4	24.5	0.122	
	930	1305.	****	35,4	24.5		
	945	1320.	****	35.4	24.5	0.118	
	1000	1335.	*****	35.4	24.5	0.116	
	1015	1350.	****		24.0	0.115	
	1030	1365.	*****	35.6	24.0	0.113	
	1045	1380.	*****	35.4	24 • C.	0.112	
	1100	1395.	*****	35.4		0.111	
	1115	1410.	*****	35.4	24.0	0.109	

		WEST - CORN THE COLD STREET, S	MARKET THE REAL PROPERTY.	and the same of th
1130	1425。 *****	35.4	24.0	0.107
1145	1440. *****	35.6	24.0	0.106
1200	1455. *****	35.6	24.0	0.105
1215	1470. 0.504	35.4	24.0	0.103

***** NO DATA TAKEN ---- DATA DISCARDED

? QUESTIONABLE DATA

AGC-218-1 SO2 40% RH GLASS CHAMBER 1976 AUG 4

(

DARK
AT 0850 FC-12 AND SOZ WERE INJECTED INTO THE CHAMBER
THE DASIB! 1212 WAS ON THE CHAMBER FROM 1651 TO 1658
BRADY 1296, CALIBRATION 1976 JUL 16
SAMPLING RATES (ML/MIN): TECO 43 - 1233; DASIB! 1212 - 600;

```
GLOCK ELAPSED TIME (MIN)
                      DZONE
                                 TS1
                                       REL HUM
                                                   502
                     (PPM)
                              IDEG C)
                                          (2)
    1100
                                 33.4
                                          49.0
                                                  0.377
    1105
                                 33.4
                                          48.5
                                                  0.391
    1110
                10.
                     ****
                                 33.4
                                          48.5
                                                  0.380
    1115
                     *****
                                 33.4
                                          46.0
                                                  0.379
    1120
                20.
                     ****
                                 33.4
                                                  0.374
    1125
               25.
                     ***
                                 33.5
    1130
                30.
                                 33.2
33.4
                                          47.5
                                                  0.371
    1135
               35.
                                                  0.372
    1140
                40.
                                 33.4
                                          46.5
                                                  0.370
    1145
                     ****
                                 33.4
                                                  0.371
                                          45.0
    1150
               50.
                     ****
                                 33.4
... 1155
               55.
                     ****
                                 33.4
                                          45.5
    1200
               60.
                                 33.4
                                          45.5
                                                  0.366
    1205
               65.
                                 33.5
                                          45.0
                                                  0.36?
                                 33.5
                70.
                                          45.0
45.0
                                                  0.359
    1215
                                 33.5
                                                  0.352
   .1220
               80.
                     ***
                                                  0.359
    1225
                     ****
               85.
                                 33.4
                                                  0.362
    1230
                     ****
               90.
                                 33.4
                                          44.0
                                                  0.362
               95.
                                          44.5
                                                  0.355
    1240
              100.
                                                  0.355
                                          44.5
    1245
              105.
                     ****
    1250
              110.
                     ****
                                 33.2
    1255
1300
                     ****
              115.
              120.
                                                  0.354
    1305
              125.
                                 33.4
                                                  0.351
                                          43.0
   1310
              130.
                                 33.4
                                          42.0
                                                  0.355
    1315
                                                  0.348
                                          42.0
    1320
              140.
                     ****
                                 33.4
    1325
                     *****
              145.
                                 33.5
    1330
              150.
                                 33.4
                                                  0.347
    1335
              155.
                                 33.5
                                                  0.344
   1340
              160.
                                 33.5
33.4
                                          42.0
                                                  0.344
    1345
              165.
                     *****
    1350
              170.
                     ****
                                 33.5
                                                  0.343
                     ****
    1355
              175.
                                 33.5
    1400
              180.
                                 33.5
                                          41.5
                                                  C.341
    1405
              185.
                                 33.7
                                          40.5
                                                  0.341
    1410
              190.
                                 33.5
33.5
                                          40.3
                                                  0.343
    1415
              155.
                                                  0.340
    1420
              200.
                     *****
                                 33.7
                     ****
    1425
              205.
                                 33.7
                                          40.5
                                                  0.338
    1430
              210.
                                33.4
33.7
                                          41.0
                                                  0.336
    1435
              215.
                     ****
                                          42.0
                                                  0.336
    1440
                     *****
                                                  0.336
    1445
                     ****
                                 33.5
   1450
1455
              230.
235.
                     ****
                                          41.5
42.0
42.0
                                                  0.332
                                 33.7
                     *****
                                33.7
                                                  0.330
    1500
              240.
                                 33.7
                                                  0.330
    1505
                                                  0.330
       ***** NO DATA TAKEN
                                          DATA DISCAPDED
                                                                  ? QUESTIONABLE DATA
```

AGC-218-2 SO2 40% RH GLASS CHAMBER 1976 AUG 4

```
CECCK ELAPSED
TIME TIME (MIN)
                          (DEG C)
                    [FP4]
           250.
                              33.7
                              33.7
 1515
           255.
                                        42.0
                                                0.325
 1520
           260.
                                        42.0
                                                0.326
 1525
1530
           265.
                  ****
                              33.7
                                        42.0
                                                0.325
           270.
                  ***
                                        41.5
                                                0.327
 1535
                  * * 4 * * *
                              33.5
                                        42.0
                                                0.324
           280.
                              33.5
 1545
           285.
                              33.4
33.4
                                        43.0
 155C
           290.
                  * * * * *
                                        43.0
 1555
           295.
                   0.003
                                        41.5
                                                C.320
 1600
           300.
                              33.4
                                        42.0
                                                0.322
 1605
           305.
                  ****
                              33.4
                                        42.0
                                                0.318
 1610
           310.
                              33.4
           315.
                              33.2
33.4
 1620
                                        42.5
                                                0.314
 1525
           325.
                  ****
                              33.4
                                       43.0
                                                0.315
 1630
           330.
                  *****
                              33.5
                                                0.315
 1635
           335.
                  ****
                              33.5
                                        43.5
                                                0.310
 1640
           340.
                              33.5
                              33.5
1645
           345.
                                        43.5
1650
1655
                              33.5
33.7
                                       44.0
43.5
                                                0.309
           355.
                  *****
                                                C.313
1700
           360.
                  ****
                              33.5
                                                0.308
1705
           365.
                  ****
                              33.8
                                                0.308
1710
           370.
                              33.8
                                       44.0
1715
           375.
                              33.7
                                       44.0
1720
           380,
                              33.8
                                       43.5
                                                0.303
1725
1730
           385.
                  *****
                              33.8
                                       44.0
                                                0.308
           390.
                  * * * * * * *
                              33.8
                                       44.0
                                                0.303
           395.
1735
                  *****
                              33.8
                                       44.0
                                                0.302
1740
           400.
                              33.8
                                                0.302
1745
           405.
                              33.8
                                       43.0
                                                0.302
1750
           410.
                              33.8
                                       43.0
                                                0.293
1755
           415.
                              33.8
                                       44.0
                                                0.299
1800
          420.
425.
                  ****
                                       43.5
                                                0.296
1805
                  マたマスキと
                              33.8
                                       43.0
                                                0.299
1811
           431.
                  ****
                             33.7
33.7
                                       43.0
                                                0.294
1816
           436.
                                       43.0
1821
           441.
                             33.7
                                       43.5
                                                0.297
1826
          446.
                                                0.297
          451.
                                               0.296
1831
                                       43.5
1836
          456.
                  ****
                              33.8
                                       43.0
1341
           461.
                             33.7
33.8
33.3
                                       43.5
                                                0.292
1846
           466.
                                       43.5
                                               0.292
1851
                  ****
                                       42.5
                                               0.292
1856
          476.
                                               0.291
          481.
486.
491.
                                       43.0
42.5
1901
                             33.8
                                               0.289
0.237
7.288
1906
                 ****
                             33.8
1911
                             33.7
                                       42.0
                                               0.287
           NO DATA
                                       DATA DISCAPDED
                                                                ? QUESTIONABLE DATA
```

```
1976 AUG 4
        CLOCK ELAPSED OZONE
TIME TIME(MIN) (PPM)
                                   TS1_
•
        1921
                    501.
                                       33.8
                                                 42.5
                                                         0.286
         1926
                    506.
                                       33.8
                                                 42.0
41.5
42.5
                                                         0.285
         1931
1936
                           ****
                                       33.7
                                                         0.285
                    516.
                           ** ***
                                       33.7
                    521.
C
         1941
                           ****
                                       33.7
                                                 41.5
                                                         0.278
         1946
                    526.
                                       33.7
33.7
                                                 41.5
                                                         0.282
         1951
                    531.
                                                 42.5
                                                         0.278
C
         1956
                    536.
                                       33.7
                                                         0.278
         2001
                    541.
                           ***
                                       33.5
                                                         0.283
         2006
                    546.
551.
                                                 42.5
Ć
         2011
                                       33.5
                                                 42.0
                                                         0.278
         2016
                    556.
                           *****
                                       33.4
                                                         0.277
         2021
                    561.
                                       33.4
33.4
                                                 42.5
                                                         0.277
C
         2026
                    566.
                                                 42.5
                                                         0.276
         2031
                                       33.4
                                                         0.278
0.275
0.274
                                                 42.0
         2036
                    576.
                                       33.4
                                                 42.5
ľ
         2041
                    581.
                           ****
                                       33.5
                                                 42.0
         2046
                                       33.5
33.7
33.5
33.7
                    586.
                                                 42.0
                                                         0.275
         2051
                    591.
                                                         0.271
                                                 43.0
C
         2056
                    596.
                                                42.5
                                                         0.271
         2101
                    601.
                           ****
                                                         0.270
         2106
                           *****
                    606.
                                                 43.0
                                                         0.271
C
         2111
                    611.
                           ****
                                       33.7
                                                         0.269
         2116
                    616.
                                       33.7
33.7
33.7
                                                         0.270
         2121
                    621.
                                                 43.0
                                                         0.270
         2126
                                                42.0
                                                         0.270
         2131
                    631.
                                       33.7
                                                 43.0
                                                         0.270
                           *****
         2136
                    636.
                                       33.7
                                                 42.5
C
         2141
                    641.
                           *****
                                       33.7
                                                42.5
                                                         0.266
         2146
                    646.
                                       33.7
                                                43.0
                                                         0.265
         2151
                    651.
                                                42.5
                                                         0.265
C
         2156
                    656.
                                       33.5
                                                         0.269
         2201
                    661.
                           *****
                                                43.0
                                                        0.266
                   666.
                           *****
                                       33.5
                                                         0.263
C
         2211
                                       33.5
33.7
                                                42.5
                                                         0.265
         2216
                    676.
                                                43.0
42.5
43.5
                                                         0.264
         2221
                    681.
                                       33.5
                                                         0.261
C
         2226
                    686.
                           ***
                                       33.5
                                                         0.263
                   691.
696.
701.
         2231
                           ****
                                       33.5
                                                43.0
                                                         0.263
         2236
                           ****
                                       33.5
                                                42.5
                                                         0.259
C
         2241
                                       33.5
                                                43.0
                                                         0.256
         2246
                    706.
                                       33.5
                                                42.5
42.5
                                                         0.258
         2251
                    711.
                           ****
                                       33.5
                                                         0.255
         2256
                    716.
                           ***
                                       33.5
                                                43.0
                                                         0.256
                                       --- DATA DISCARDED
                    NO DATA TAKEN
                                                                         ? QUESTIONABLE DATA
```

AGC-218-3 SO2 40% RH GLASS CHAMBER

1000

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THE PARTY NAMED OF

· 大部分編集

大田 大田 本

Towns of

AGC-218-4 502 40% RH GLASS CHAMBER 1976 AUG 4-5

# ADO 660 MIN TO ELAPSED TIME

	CLCCK	ELAPSED	TS1	REL HUM	502	
	TIME	TIMEIMINI		(3)	(PPM)	·
	2206	6.	33.5		0.263	"
				42.5		
	2211	11.	33.5	42.5	C.265	
1 100 11	2216	16.	73.7	43.0	0.264	
	2221	21.	33.5	42.5	0.261	
	2226	26.	33.5	43.5	0.263	
	2231	31.	33.5	43.0	0.263	•
	2236	36.	33.5	42.5	0.259	<ul> <li>A control of the contro</li></ul>
	2241	41.	33.5	43.0	0.256	
	2246	46.	33.5	42.5	0.253	The second of th
	2251	51.	33.5	42.5	0.255	
	2256	56.	33.5	43.0	0.256	
	2301	61.	33.5	42.5	C.254	
	2306	66.	33.5	42.5	C.255	
	2311	71.	33.5	43.0	C.250	•
	2316		33.7	42.5	0.250	The same of the same of the same and a same of the sam
	2321	81.	33.5	43.0	0.250	•
	2326	86.	33.5	43.3	0.252	
	2331	91.	33.4	42.0	0.249	•
	2336	96.	33.5	43.0	C.250	The state of the s
	2341	101.	33.5	42.5	C.252	
	2346	106.	33.5	42.0	0.245	
						The street of section of the street of the section
	2351	111.	33.5	42.5	0.248	
	2356	116.	33.4	42.0	0.248	A contract of the contract of
	1	121-	33.4	42.5	0.247	
	6	126.	33.4	42.5	C+250	The second secon
	. 11	131.	33.4	42.0	0.244	•
	16	136.	33.4			
	21	141.	33.4	42.0	0.244	The second secon
	26					and the second s
		146.	33.4	42.0	0.244	•
	31	151.	33.2	42.0	0.242	
	36	156.	33.4	41.5	0.242	· · · · · · · · · · · · · · · · · · ·
	41	161.	33.4	42.5	0.241	
	46	166.	33.2	42.0	0.239	
	51	171.	33.4	43.0	0.239	· ·
	56	176.	33.2	43.0	0.239	· ·
	101	181.	33.2		0.236	
				42.5		
	106	186.	33.2	43.5	C.236	
	111	191.	33.2	43.0	0.238	
	116	196.	33.1	43.0	0.236	
	121	201.	33.2	43.5	0.234	
	126	206.	33.2	43.0	0.233	
	131	211.	33.2	43.5	0.232	
	136	216.	33.2	43.0	0.233	·
	141					
		221.	33.2	42.5	0.233	•
	146	226.	33.2	43.5	C.233	•
	151	231.	33 <b>.</b> l	42.5	C.228	
					•	•
						And the second s
	156	236.	33.2	43.5	C.228	•
	201	241.	33.1	43.0	0.230	
	206	246.	33-1	43.5	0.230	
	211	251.	33.1	44.0	0.230	
				•	_	
	**	**** NO D	ATA TAKE	·	DATA	DISCAPCED ? QUESTIONABLE DATA

AGC-218-5 SO2 40% RH GLASS CHAMBER 1976 AUG 5

ADD 660 MIN TO ELAPSED TIME

Commence of the second second

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CLOCK ELAPSED
                      TSI
                              REL HUM
(%)
                                           502
TIME
       TIME (MIN) (DEG C)
  216
            256.
                       33.1
                                 43.0
  221
            261.
                      33.1
                                 44.5
                                          C.230
            266.
271.
276.
  226
                       33.0
                                 43.5
                                          0.227
                                44.0
44.5
43.5
                                          0.228
                      33.0
33.0
  231
  236
  241
            281.
                       33.0
                                          0.226
  24,6
            286.
                       33.0
                                 44.5
  251
            291.
                       33.0
                                 43.5
            296.
  256
                      33.0
                                 43.5
                                          0.223
  301
                                 44.0
                                          0.225
  306
            306.
                       32.8
                                 43.5
                                          0.225
  311
            311.
                                 44.5
                                          0.226
                       32.8
  316
            316.
                       32.7
                                          C.222
  321
            321.
                       32.8
                                          0.222
  326
            326.
                       32.8
                                 43.5
                                          C.221
  331
            331.
336.
341.
346.
                       32.8
                                 43.0
43.5
                                          0.223
  336
                       32.8
32.8
32.8
                                          C.220
0.217
  341
                                 43.0
                                 44.0
                                          0.220
  351
            351.
                       32.8
                                 43.5
                                          C.220
  355
                       32.7
32.7
32.7
            356.
                                 44.5
                                          0.217
C.217
            361.
  406
            366.
                                 44.0
                                          0.216
  411
            371.
                       32.7
                                          0.215
  416
            376.
                       32.6
                                          C.217
  421
            381.
                       32.7
  426
            386.
                       32.6
                                 44.0
            391.
  431
                                 44.5
                       32.6
                                          0.211
  436
            396.
                       32.5
                                          0.211
            401.
                       32.6
  441
                                 45.0
                                          0.210
            406.
                                 44.0
  451
            411.
                       32.4
                                 45.0
                                 44.5
45.5
44.5
  456
            416.
                       32.4
                                          C. 210
  501
            421.
                                          0.211
  506
            426.
                       32.3
                                          C.210
  511
            431.
                       32.3
                                 45.5
                                          0.204
   516
             436.
                       32.3
                                          0.209
  521
            441.
                       32.3
                                 45.5
  526
531
            446.
451.
                       32.3
32.3
32.3
                                 44.5
                                          C - 20,8
                                 45.5
                                          0.208
   536
            456.
   541
             461.
                       32.2
                                 45.5
                                          0.208
   546
            466.
                       32.2
                                 44.5
                                          0.205
  551
            471.
                       32.2
                                 45.0
                                          3.236
  556
601
            476.
                       31.6
31.6
                                 45.0
                                          0.210
            481.
                                          0.205
  606
            486.
                       31.6
                                 45.5
45.5
                                          0.203
0.202
0.202
  611
             491.
             496.
                       31.6
                                 45.0
   153
             501.
              NO DATA TAKEN
                                         -- DATA DISCARDED
                                                                      7 QUESTIONABLE DATA
```

AGC-218-6 SO2 40% RH GLASS CHAMBER 1976 AUG 5

# ADD 660 MIN TO ELAPSED TIME

τ (	<b></b>		ELAPSED TIME(MIN)	TS1 (DEG C)	REL HUM	SO2 (PP4)		on Maria — a seen a shinga a seenaan a	<b>mana</b> and a gran			e Control debut with the		. 🔪	N. 11
<b>(</b> ·		626 631 636	506. 511. 516.	31.6 31.6 31.6	46.0 45.5 45.5	0.200 0.200 0.200		AND AND AND AND AND A				a to communication of the comm			•
C	<u>د</u>	641 646 651	521. 526. 531.	31.6 31.5 31.6	46.0 45.0 45.5	0.199 0.199 0.199							•	THE R PART AND A	
C		656 701 706 711	536. 541. 546.	31.5 31.8 31.9	45.5 45.0 45.5	0.195 0.197 0.197	N= 8-1-2-a , an		and Man Make a said						
•	•••	716 721 726	551. 556. 561. 566.	31.9 32.0 32.2 32.3	45.5 45.5 46.0 45.5	0.195 0.199 0.197 0.195		THE STREET OF STREET STREET		•			· .		
(		731 736 741	571. 576. 581.	32.4 32.4 32.4	45.5 45.5	0.194 0.195 0.193					F				
C		746 751 756	586. 591. 596.	32.6 32.7 32.8	45.0 45.5 45.5	0.192 0.194 G.194									
SHOWK	·	801 806 811	601. 606. 611.	33.0 33.1 33.1	45.5 46.0 45.0	0.193 0.191 0.191		<del></del>					-		. Name of the second of the se
(	ras dag r	816 821 826 831	616. 621. 626. 631.	33.2 33.2 33.4 33.4	45.0 45.5 46.0	0.191 0.192 0.183	NYDT THE CHICAGO MANNEY	44	e - adapte - age a			e non electrical			
(		836 841 846	636. 641. 646.	33.4 33.5 33.5	45.5 45.0 45.0 46.5	C.188 C.188 C.188 C.187			<del> </del>	<del></del>					
(		851 856	651. 656.	33.5 33.5	45.5 45.0	C.136 0.184	en e			-			Milyani dan 18 km yan da	e on the second subdents	·
(		**	**** NO DA	TA TAKE		DATA	DI SCARD	ED ·	7 CUEST	IONABLE I	ATA		int from the second second		
(	40° au	who type to make the con-				Nijedija a postovana tepi p pa	alarin i ilah kalandara da kala		- myreter and a common		eli Pi Lacher Sphae Pi Name - 19 c 1996 s				
(			ere eremen gift i it i venn jurenn var i sich die ge		The second second second second second								*****		*******

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AGC-218-7 SO2 404 PH
               GLASS CHAMBER
              1976 AUG 5
     LIGHTS EN 0900: INTENSITY 100%

THE DASIBITIATE WAS ENTIFE CHANGES: AUGS 0906 TO 0911, FROM 1 MIN TO 5 MIN AFTER
THE HOUR FROM 1000 TO 1906, 2047 TO 2130, 2201-2205; AUG 6 0707-0710

BESARY 1296, CACLUSATION 1976 OUT 16

SAMPLING RATES (MEAMIN): TECH 43 - 1233; CASIEI 1212 - 600;
     CLOCK ELAPSES CZCNE (1151 REL HOM TIME TIME(MIN) (FPM) (CEC C) (6)
            901
                                                      45.5
                               ***
                                            33.5
                                                                0.100
            906
                                            33.7
                         6.
                                                                0.105
                                            34.2
34.5
            211
                                                       55.5
                                                                <u>C.142</u>
C.150
0.177
                        11.
                                                       49.5
            921
                               ****
                        21.
                                            34.9
            926
                               各种特别形象
                        2t.
                                            34.9
                                                       44.5
44.0
                                                                0.170
            931
                        31.
                                                                0.175
            935
                        36.
                               224244
                                            35.1
                                                       43.5
                                                                0.173
            941
                        41.
                               ****
                                                       42.5
                                                                0.171
                               ****
            940
                        46.
(
            951
                               *****
                        51.
                                            34.5
                                                       42.0
                                                                0.166
            956
                               *****
                        50.
                                            34.5
           1001
                        cl.
                                                                0.164
           100c
                                0.114
                                            34.5
                        ćć.
                                                       41.5
                                                                C.145
           1011
                        71.
                                            34.7
                                                       41.0
42.0
                                                                0.164
           1016
                               ****
           1021
                              ***
                        81.
                                            34.5
                                                       42.0
           1026
                               ***
                        Se.
                                            ئ. 4د
                                                                C.155
           1031
                        91.
                                            34.5
                                                       41.0
                                                                0.158
           1036
                        96.
                               ****
                                            34.5
                                                       40.5
                                                                0.156
           1041
                       101.
                               ត្រូវ មាន ក្រុង ស
                       106.
           1046
                               ****
.(
           1051
                              *****
                       111.
                                            34.7
                                                       40.5
                                                                0.14%
           1056
                               ****
                                            34.0
                                                       41.0
                       116.
           1101
                       121.
                                                                0.151
                                                       41.0
C
           1106
                       126.
                                0.170
                                            34.0
                                                       40.5
                                                                0.153
           1111
                       131.
                                            34.5
                                                       40.0
                                                                0.140
                               ****
                       136.
           1121
                       141.
                              *****
                                            34.0
                                                       39.5
                                                                0.146
           1120
1131
                       146.
                                            34.0
                                                       34.0
                                                                0.147
                       151.
                               ****
                                                       39. ŭ
                                                                0.143
           1136
                       156.
                              ****
                                                       39.C
                                                                0.142
           1141
                       lol.
                              ****
                                                       36.5
                                            34.6
                       166.
                              ****
C
           1151
                              ****
                       171.
                                            34.6
                                                       37.5
                                                                0.139
           1156
                       176.
                               *****
                                            34.5
34.6
                                                       37.0
                                                                0.140
           1201
                       lal.
                                                       36.5
                                                                0.138
          1206
                       136.
                                0.206
                                            34.6
                                                       35.0
                                                                0.137
           1216
                      151.
                               ****
                       201.
           1221
                                            34.4
                                                      34.0
                                                                C.133
                              ****
                                            34.5
                                                       34.0
                                                                0.123
           1231
                      211.
                              ****
                                                       32.3
                                                                6.134
           1236
                      216.
                              *****
                                            34.0
                                                       33.0
                                                                0.130
                       221.
           1241
                       226 .
                                                                0.128
Ų,
(
                      231.
                                           34.0
           1251
                                                      23.5
33.0
                                                               0.129
1250
                      236.
           1301
                       241 -
                              ****
                                                       1: 5
                                                                1.120
           1306
                      240.
                                3.239
               PARKAR DIA DAKEN
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for company of

AGC-218-8 SO2 40% RH GLASS CHAMBER 1976 AUG 5

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REL HUM
      CLECK
               ELAPSED
                                     TS1
             TIME (MIN)
                          (PPM)
                                  (DEG C)
                                              (%)
                                                       (PPM)
       TIME
                                     34.5
                                               33.0
                                                       0.125
                  251.
        1311
                                     34.5
                                               33.5
                                                       0.129
        1316
                  256.
                  261.
                         ***
                                               32.5
                                                       0.123
        1321
        1325
                  266.
                          * * * * * * *
                                     34.7
                                              33.5
                                                       0.123
        1331
                  271.
                          ****
                                     34.9
                                               34.0
                                                       0.122
                                                       0.122
                                               34.0
        1336
                  276.
                          *****
                                     34.7
                          ****
                                     34.7
        1341
                  281.
                          ***
                                     34.7
                                               34.5
                                                       0.120
        1346
1351
                  286.
                                     34.7
                                               36.0
                                                       0.120
                  291.
        1356
                          ****
                                     34.6
                                               36.C
                                                       0.118
                  296.
                                               35.5
35.5
        1401
                  301.
                          ****
                                     34.6
                                                       0.117
                           0.264
                                     34.6
                                                       0.118
        1406
                  306.
                                               34.0
                                                       0.118
                                     34.6
        1411
                  311.
                          *****
                                     35.0
                                               35.5
                                                       0.118
                   316.
        1421
                   321.
                          ****
                                     35.1
                                               36.0
                                                       0.117
                   326.
331.
                                     35.1
35.0
        1425
                          *****
                                               35.5
                                                       0.116
                                               33.5
        1431
                          ***
                                                       0.114
                                               35.0
                                     35.4
35.4
                          ****
                                                       0.114
        1436
                   336.
                          ****
                                               35.5
                                                       0.111
        1441
                   341.
                                               35.5
                                      35.4
                                                       0.112
        1446
                   346.
                   351.
                          ****
                                      35.3
                                               35.0
                                                       0.110
        1451
        1456
                   356.
                          *****
                                      35.1
                                               36.0
                                                       0.111
                                     35.1
35.0
35.0
34.9
                                               34.5
34.5
        1501
                   361.
                          ****
                                                       0.110
                                                       0.109
                           0.287
        1506
                   366.
                          ****
                                               34.5
                                                       0.109
        1511
1516
                   371.
376.
                                               34.0
                                                       0.109
        1521
                   381.
                          *****
                                      34.7
                                               34.0
                                                       0.109
                                               35.5
36.0
        1526
                   386.
                          ****
                                      34.7
                                                       0.107
                                                       0.107
                          ****
                                      34.7
        1531
                   391.
                          ****
                                      34.6
                                               36.5
                                                       0.104
        1536
1541
                   396.
                   401.
                                      34.6
                                               36.C
                                                       0.106
        1546
                          ****
                                      34.6
                                               36.5
                                                       0.104
                   406.
        1551
                   411.
                          ****
                                      34.5
                                               36.5
                                                       0.104
                                               36.5
36.5
36.0
                                                       0.104
         1556
                          ****
                                      34.6
                                                       0.103
                          ****
         1601
                   421.
                                      34.5
                   426.
431.
                           0.302
                                      34.6
                                                       0.103
         1606
                                      34.5
                                               36.5
                                                        0.100
         1611
                          ****
                                      34.5
                                               37.5
                                                       0.100
                   436.
         1616
         1621
                   441.
                          *****
                                      34.5
                                               37.0
                                                       0.100
                          *****
                                      34.5
                                               36. C
                                                       0.098
         1626
                   446.
                   451.
                          *****
         1631
                                               36.0
                   456.
461.
                          ****
                                      34.5
                                               35.5
                                                        0.098
         1636
         1641
                                      34.5
                                               37.C
                                                        0.098
         1646
                          ****
                                      34.5
                                               36.5
                                                        0.094
                   466.
         1651
                   471.
                          ****
                                      34.5
                                               37.0
                                                        0.094
                                                        0.094
         1656
                   476.
                          *****
                                      34.5
                                               37.0
         1701
                   481.
                                      34.5
34.5
34.5
                                                36.0
                                                       0.095
43
                           0.315
                                                30.0
                   491.
                                                35.5
                                                        0.094
         1711
         1716
                    496.
                           *****
                                                34.5
                                                        0.092
                                                                        ? QUESTIONABLE DATA
            ***** NO DATA TAKEN
                                                DATA DISCAPDED
```

#### AGC-218-9 502 40% RH GLASS CHAMBER 1976 AUG 5

# AT 2059 PROPENE (6.4 ML) AND FC-12 (58.0 ML) WERE INJECTED

€,	61.064	F				
		ELAPSEO_			REL HUM	S.J2
-	TIME	TIME (MIN)	(BBM)	(DEG C)	(%)	(PPM)
C				٠.		•
		د درو وساست				
-	1721	501.	****	34.5	34.0	0.092
C	1726	506.	****	34.5	34.0	0.092
	1731	511.	****	34.5	34.5	0.092
	1736	516.	*****	34.3	35.0	0.089
C.	1741	521.	****	34.3	33.5	0.089
	1746	526.	*****	34.5	33,0	0.088
-	1751	531.	****	34.6	31.0	0.087
C	1756	536.	****	35.0	30.5	0.035
	1801	541.	****	35.1_	32.0	0.085
	1806	546.	0.313	30.0	33.0	0.084
Ċ	1811	551.	****	35.8	32.0	0.085
-	1816	556.	****	35.8	32.0	0.081
3	1821		****	35.8	32.0	0.083
ξ(	1826	566.	****	36.0	31.5	0.083
t Je Bosness Fr	1831	571.	***	35.)	31,5	0.083
1	1836	576.	****	36.0	32.0	0.381
£ (	1841	581.	****	38.0	31.5	0.078
3	1846	586.	****	38.0	32.0	0.081
	1851	591.	****	37.9	33.0	0.079
C	1856	596.	****	37.7	33.5	0.078
	1901	6.01	*****	37.6	33.0	0.078
	1906	606.	0.328	37.5	34.0	0.078
Ĺ	1911	611.	****	37.5	33.5	0.078
	1916	616.	* * * * * *	37.6	33.0	0.076
	1921	621.	****	37.6	33.0	0.077
C	1926	626.	****	37.5	33.5	0.077
	1931	631.	****	37.6	34.0	0.074
_	1936	636.	****	37.5	34.5	0.070
C	1941	641.	* * * * * *	37.2	34.5	0.274
	1946	646.	****	37.2	34.0	0.074
_	1951	651.	****	37.2	34.0	0.074
(	1956	656.	****	37.2	34.5	0.073
	2001	661.	****	37.0	35.0	0.071
-01	2006	666.	****	37.0	35.0	0.072
C	2011	671.	***	36.9	35.5	0.071
	2016	676.	****	36.9	35.5	0.068
- 1-	2021	681.	****	36.0	36.0	0.068
C	2026	686.	****	34.9	36.5	0.069
	2031	691.	****	34.9	36.5	9.070
,	2036	696.	****	34.9	37.0	0.066
(	2041	701.	****	35.0	37.0	0.066
	2045	706.	*****	34.9	38.0	0.065
	2051	711.	0.341	35.0	38.0	0.066
C	2056	716.	0.341	35.0	38.5	0.066
	2101	721.	0.343	33.7	38.5	0.066
		·				

AGC-218-10 SO2 40% RH GLASS CHAMBER 1976 AUG 5-6

ADD 720 MIN TO ELAPSED TIME AT 2059 PROPENE (6.4 ML) AND FC-12 (58.0 ML) WERE INJECTED AT 2217 1.0 ML OF SG2 WAS INJECTED

CLOCK TIME	CERTAPSED (NIM) SMIT	OZONE (PPM)	TS1	REL HUM (%)	\$02 (PPM)		
2106	6.	0.328	34.5	39.0	0.062		A Committee of the Comm
2111	11.	0.314	34.9	39.0	0.060		
2116	16.	0.300	34.9	39.0	0.360		agripping of the annual contract of the property of the annual of the state of
2121	21.	0.290	34.9	39.0	0.057	•	
2126	26.	0.281	35.0	39.0	0.056		
2131	31.	0.282	35.0	39.40	, 0.C55,		e and a great and a second special and a second
2136	- 36.	****	35.0	39.0	0.056		
2141	41.	****	35.0	39.0	0.054		
2146	46.	****	35.0	39.0	0.054		
2151	51.	***	35.0	39.0	0.051		
2156	56.	***	35.0	39.0	0.053		
2201	61.	*****	35.0	39.5	,0.053		
2206	66.	0.241	35.0	39.5	0.051		
2211	71.	****	35.0	39.0	0.051		
2216	76.	***	35.0	39.5	0.050		naga - Agramming St. 1750 companya regiong par in 16 ap. given 150 ap. given a second membranya panaman and a consequent
2221	81.	***	33.8	39.0	0.216		• •
2226	85.	****	34.7	39.5	0.222		
2231	91.	****	34.9	39.5	0.222		
2236	96.	***	34.9	39.0	0.221		
2241	101.	***	35.0	39.0	0.217		
2246	106.	*****	34.9	38.5	C.220		
2251	111.	****	34.9		0.220		
2256	116. _p	****	35.0	39.0	0.219		
2301	121.	****	34.9	39.0	0.216		E A MANUSCO E CARA COMA MARCAMANICAMA MARCANICA CON TRACTOR MILITARIO E A CA-MORALISMO ATTOR
2306 2311	126.	*****	34.9	38.5	0.214		
		****	34.9	38.5	0.213		
2316 2321	136.	****	34.9	39.0			
2321	146.	****		39.0	0.209		
2331		****	34.7 34.7	39.0	0.209		
2336	156.	****	34.7	38.5 39.0	0.206	-	The state of the second control of the second control of the second of t
2341	161.	****	34.7	39.0	0.204		
2346			34.7	39.0	0.204		
2351	171.	****	34.7	38.5	0.204		
2356	176.	***	34.7	38.5	0.203		
1	181.	*****	34.6	39.0	0.198		
6	186.	****	34.6	39.5	0.198		The state of the s
11	191.	****	34.5	39.0	0.200		
16	196.	****	34.5	38.5	9.198		· · · · · · · · · · · · · · · · · · ·
21	201.	* * * * * *	34.5	38.5	0.195		The section of the se
26	206.	****	34.5	39.0	0.195		
31	211.	****	34.5	39.0	0.194		
36	216.	****	. 34.5	39.0	0.194		
41	221.	****	34.3	38.5	0.191		
46	226.	****	34.5	38.5	0.191		
51	231.	*****	34.3	39.0	0.192		
							•
	•						
56	235.	*****	34.3	39.0	0.187	1	'
101	241.	***	. 34.3	38.5	0.188		
106	246.	****	34.3	38.5	0.189		
111	251.	***	34.3	38.5	6.134		
*	***** %g D	ATA TAK	EN -	DATA	DISCARD	030	? QUESTIONABLE DATA

AGC-218-11 SO2 40% RH GLASS CHAMBER 1976 AUG 6

# ADD 720 MIN TO ELAPSED TIME

	CLOCK TIME	ELAPSED TIME(MIN)	OZCNE (PPM)	TS1 (DEG C)	REE HUM (%)	SC2 (PPM)	
	116	256.	***	34.3	38.5	0.100	and the second of the second o
	121	261.	****	34.3	38.5	0.183 0.184	•
	126	266.	****	34.3	38.0	0.154	
	131	271.	***	34.2	38.5	0.181	the second secon
	136	276.	****	34.2	38.5	0.182	
	141	291.	****	34.2	38.C	0.180	
	146	286.	***	34.2	38.0	0.177	1 P. 1 P. 1
	151	291.	***	34.2	38.0	0.176	• • • •
	156	296.	***	34.2	38.5		
	201	301.	***	34.2	38.0	0.176	The second control of
	206	306.	****	34.2	38.C	0.175	,
	211	311.	*****	34.2	38.C	0.172	
	216	316.	***	34.2	38.5	0.173	
	221	321.	****	34.2	38.5	0.171	• •
	226	326.	****	34.1	38.5	0.169	
	231	331.	****	34.1	38.5	0.169	the state of the s
	236	336.	****	33.9	39.0	0.165	
	241	341.	****	33.9	38.5	C-170	
	246	346.	****	33.9	35.5	0.170	The control of the co
	251	351.	***	33.9	38.5	0.165	•
	256	356.	*****	33.9	39.0	0.167	
	30 L	361.	***	33.9	33.5	0.166	and the second s
	306	366.	****	33.9	33.5	0.164	
	311	371.	***	33.9	38.5	0.161	
	316	376.	****	33.9	38.5	C.161	The state of the second section of the section of the second section of the secti
•	321	381.	****	33.9	38.0	0.163	
	326	386.		33.48	38.0	0.161	
	331	391.	****	33.8	38.5	0.161	
	336	396.	****	33.8	38.5	0.158	
·	341	401	****	33.8	39.0	0.159	
	346	406.	****	33.8	38.5	0.156	
	351	411.	***	33.8	38.5	9.156	
	356 401	416.	****	33.8	38.0	0.156	MANAGER STATE OF A STATE OF STATE OF STATE OF THE STATE O
	401	421. 426.	***	33.8	38.5	0.151	
	- 411	431.	****	33.8	38.5	0.153	
****	416	436.	*==**	33.6	39.0	0.153	The server of the country of the server of t
	421	441.	****	33.8 33.8	38.0	0.153	
	426	446.	****		38.5	0.151	•
	431	451.	*****	33.8 33.8	38.0	0.149	The print and the state of the
	436	456.	***	33.8	38.5	0.150	•
	441	461.	****	33.7	38.5	0.148	
4 1 1	446	466	****	33.8	36.5	0.143	The state of the s
ĺ	451	471.	*****	33.7	39.0	0.145	
•	456	476.		33.8	39.0	0.144	
	501	481.	***	33.7	38.5	0.148	Approximate the second contraction and the second contraction of the s
				224,	.,,•,	0.140	
		The state of the state of	• · ·			te i i ii	e de la Electrica de la Companya de
	506	486.	****	33.8	38.5	0.143	
	511	491.	****	33.7	38.5	C-140	
	516	496.	****	33.8	38.0	0.142	
	521	501.	*****	33.8	38.0	0.139	
	. **	**** NO DA	TA TAKE	ı	DATA	DISCAPDE	D ? QUESTIONABLE DATA

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AGC-218-12 502 405 RH
               GLASS CHAMBER
               1975 AUC 5 . .
        ACD 720 FIN TO ELAPSED TIME
      CLCCK BLARSEC DIONE TSI BEL HUM SOZ
TIME TIME(MIN) (PPN) (DEG C) (E) (PPN)
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                      526.
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                      531.
                              *****
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                              40 $ $ $ $ $ $
                      536.
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            601
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                      541.
                                           33.7
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35.5
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                     676.
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686.
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                                                             0.111
           826
                                                    38.5
           831
                      691.
                             ****
                                          34.2
                                                             5.114
              ***** NO SATA TAKEN
                                               ---- GATA DISCAPDED
                                                                               7 LUESTICNABLE CATA
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### AGC-218-13 502 40% RH GLASS CHAMBER 1976 AUG 6

ADD 1410 MIN TO ELAPSED TIME

	CLOCK	ELAPSED TIMELMINI	020NE [PPM]		REL HUM	SOZ (PPM)		mangers of promisional states of the	
									***
	829	-1.	****	34.2	39.0	0.114			
	836	.6.	****	33.9	39.0	0.115			
	. 841	11.	***	33.9	39.5 40.0	0.114			
	846	16.	*****	33.8		3.112			
	851 856	21. 25.	****	33.7 33.7	40.0 40.0	0.116			
٠.	901	31.	****	33.7	39.0	0.112	, the state of the		• • • • • • • • • • • • • • • • • • • •
	901	36.	****	33.8	38.0	C.110			
	911	41.	***	34.1	37.0	0.109			
	916	46.	****	34.3	37.0	0.107	on the second of the temporary contract on the		·
	921	51.	****	34.5	36.5	0.106			
	926	56.	****	34.7	36.5	0.105			
	931	61.	***	34.7	38.0	0.104			
	936	66.	****	3+.5	38.5	0.103			1
	941	71.	****	34.5	38.5	0.104			
	946	76.	***		78.5	0.105			
	951	81.	*****	34.2	38.5	G.104			
	956	86.	****	34.1	38.5	0.103			
•• •	1001	91.	****	33.9	38.0	0.103			
	1006	96.	****	33.9	37.5	0.105			
	1011	101.	****	33.9	37.5	0.101			
-	1016	106.	****	33.9	38.0	0.099			
	1021	111.	****	33.9	38.0	0.099		4	
	1026		****	33.9	37.0	0.101			
	1031	121.	****	33.9	37.0	0.096	the contract of the contract o		
	1036	126.	****	33.9	37.0	0.096			
	1941	131.	****	33.9	37.5	0.099		i .	100
	1046	136.	****	34.1	37.5	0.098		AND A TAX TO A CARDON MARK TO A STATE OFFICE A	
	1051	141.	****	33.9	37.0	0.098		*	
	1056	146.	****	33.9	37.0	0.095			
	1101	151.	***	34.1	37.5	0.094	1 1		•
	1106		****	34.2	37.C	0.095			
	1111	161.	****	34.2	37.C	0.093			
	1116	166.	****	34.2	36.C	0.096			
	1121	171.	****	34.2	36.C	0.093			
	1126		****	34.2	36.5	0.094			
-	1131		****	34.2	36.5	0.094			4
	1136		***	34.2	. 36.C	0.090			
	1141	191.	***	34.3	35.0	0.094			
•	1146		****	34.3	35.C	0.000			
	1151		****	34.3	34.0	0.089		•	
	1156		***	34.3	34.0	0.089			
	1201		****	34.3	33.5	0.692			
	1206		*****	34.3	33.0	0.037	,		
	1211	271.	****	34.5	33.0	0.589			
	1216		****	34.5	32.0	0.089			
						100			
							-		
			4						
	1221	231.	****	34.5	32.5	0.083			•
	1226	236.	***	34.5	31.5	0.087			
	1231		* = * * * *	34.5	31.0	0.084			
	1236	246.	*****	34.5	30.5	0.387			
. ~~		**** 40 [	ATA TAK	EN	DATA	DISCAPE	18. 1	JOST LONABLE DATA	Λ

AGC-218-14 SD2 40% RH GLASS CHAMBER 1976 AUG 6

ADD 1410 MIN TO ELAPSED TIME AT 1424 1 ML CF SO2 AND 1.6 ML OF PROPENE WERE INJECTED CLIMET AND WHITEY WERE ON THE CHAMBER FROM 1313 TO 1645 DASIBI 1212 WAS ON THE CHAMBER FROM 1634 TO 1638

	1631	481.	农力有象准尔	35.0	31.5	0.181	9 9 9 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
	1020	710.	*****	35.0	31.0	0.184	•
٠	1626	471. 476.	****	35.0 35.0	29.5 31.0	0.184	
	1616 1621	466.	*****	35.0	29.5	0.186	
	1611	461.	****	35.0	30.0	0.191	
	1606	456.	<b>表本意识式</b> 20	35.0	31.0	0.194	
	1601	451.	****	35.0	31.5	0.192	·
	1556	446.	****	34.9	32.0	0.195	
	1551	441.	****	35.0	32.0	0.198	
	1546	4.36	*****	34.9	32.5	0.202	
•	1541	431.	****	34.9	33.0	0.202	
	1535	426.	***	34.9	33.5	0.202	
	1531	421.	****	34.9	33.5	0.206	
	1526	416.	*****	34.9	34.0	0.211	A Arrango Company
	1521	411.	*****	34.7 34.7	35.0 35.0	0.214	
	1511 1516	401. 406.	*****	34.7	35.0	0.217	,
	1506	396.	*****	34.7	34.5	0.221	
	1501	391.	****	34.7	34.5	0.222	* .
	1456	386.	****	34.7	34.0	0.223	
	1451	381.	****	34.7	34 • 0		
	1446	376.	****	34.6	33.5	0.228	A second
-	1441	371.	***	34.6	33.5	0.231	to the second district a second start to be second training a second district and the second district and second s
	1436	366.	****	34.5	32.0	0.232	
	1431	361.	****	34.3	31.0	0.221	
	1426	356.	*****	33.1	31.0	0.373 C.138	res and the implemental that is defined the implementation according to the implementation of the contract of
	1421	351.	****	34.7 34.6	30.5 31.0	0.071	
	1411	341. 346.	****	34.6	30.C	0.072	
	1406	336.	*****	34.6	. 29.5	0.073	The second secon
Ċ	1401	331.	****	34.6	29.0	0.373	
	1356	326.	****	34.5	29.0	0.073	
	1351	321•	****	34.5	30.0	0.073	
	1346	316.	****	34.6	29.5	0.077	
	1341	311.	*****	34.6	29.5	0.078	The second of th
	1336	306.	****	34.5	31.5	0.078	
	1331	301.	***	34.5	31.5	0.082	
	1326	296	**=**	34.5	31.5	0.082	
	1321	291.	****	34.5	30.5	0.081	
	1316	286.	*****	34.6 34.6	31.5 31.0	0.083	• •
	1305	276.	****	34.6	31.5	0.083	
	1301	271.	****	34.7	32.5	0.083	
	1256	266.	***	34.7	32.5	0.032	•
	1251	261.	****	34.9	31.5	0.087	
	1246	256.	*****	34.9	32.0	0.084	
	1241	251.	***	34.9	32.0	0.035	

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AGC-219-1 SOZ 808 RH
GLASS CHAMBER
              1976 AUG 16
     DARK
        AT 1545 FC-12 WAS INJECTED INTO THE CHAMBER
        AT 1646 SO2 WAS INJECTED INTO THE CHAMMER
TECO 43 SPANNED BASED ON CHAMBER INJECTION
TECO 43 SAMPLING RATE 1233 ML/MIN
        BRACY 1296, CALIBRATION 1976 JUL 16
            SOZ CORRECTION -0.1184 PPM
         CLCCK ELAPSED TS1 REL HUM SOZ
TIME TIME(MIN) (DEG C) (%) (PPM)
           1733
                        3.
           1735
                        5.
                                32.6
                                                  0.237
                                          81.5
           1740
                       10.
                                                  0.290
                                32.9
           1745
                       15.
                                          81.5
                                                  0.295
           1750
                       20.
                                32.6
                                          81.5
                                                  0.297
                       25.
                                32.6
                                          81.5
                                                  0.302
           1755
           1803
 C
           1805
                                                  0.303
0.307
                       35.
                                32.7
                                          81.0
                                32.7
           1810
                       40.
                                          81.0
           1815
                       45.
                                32.3
                                          91.0
                                                  0.303
 C
           1820
                       50.
                                32.7
                                          61.0
                                                  0.304
           1825
                       55.
                                32.7
                                                  0.304
           1830
                       60.
                                33.0
                                          80.5
                                                  0.302
           1835
                       65.
                                32.8
                                          83.5
                                                  0.302
                                                  0.302
           1840
                       70.
                                32.7
                                          80.5
           1345
                        75.
                                33.0
                                          80.5
                                32.7
                                                  0.303
           185C
                       80.
                                          80.5
                       85.
                                32.7
                                          80.5
                                                  0.297
           1900
                       90.
                                                   0.297
³ C
           1905
                       95.
                                33.2
                                          80.5
                                                  0.292
                                33.2
33.1
                                          80.5
           1910
                      100.
                                                   C.292
           1915
                                                  0.292
                      1C5.
 C
           1920
                      110.
                                33.1
                                          80.5
                                                  C.290
           1925
                                          80.5
                      115.
                                33.1
           1930
                      120.
                                                   C.293
                                                  0.285
 C
           1935
                      125.
                                33.1
                                          80.5
           1940
                      130.
                                33.1
                                          83.5
                                                   C.293
                                                   C.282
           1945
                      135.
                                33.0
                                          80.5
           1950
                                33.0
33.0
                      140-
                                          83.5
                                                  0.281
                                          80.5
                                                   C.281
                      145.
           2000
                      150.
                                 32.8
                                          80.5
           2005
                      155.
                                33.0
                                          80.5
 (
           2010
           2015
                      165
                                32.8
                                          80.5
                                                   0.275
                                                  0.272
0.266
0.272
           2020
                      170.
                                32.8
                                          80.5
                      175.
                                33.0
32.8
           2025
                                          80.5
           2030
                                          79.5
                                                   C.263
           2035
                      185.
                                33.4
 C
                                          79.3
78.5
           2040
                      190.
                                                   0.269
           2045
                      195.
                                 33.5
 (
           2050
                      200.
                                33.8
                                          77.0
                                                   0.253
           2055
                      205.
                                33.8
                                          76.5
                                                   0.260
                                                   C.254
C.258
           2100
                      210.
           2105
                      215.
                                          76.5
                                33.9
           2110
                      220.
 (
           2120
                      230.
                                           76.¢
                                                   C.253
                                          76.0
 2125
                      235.
                                34.2
                                                   0.250
           2130
2135
                      240.
245.
                                34.1
                                           76.0
                                                   0.250
                                           76.0
                                                   0.24 )
                                                 --- CATA DISCARDEU 7 QUESTIONABLE DATA
               ***** NO DATA TAKEN
```

```
AGC-219-2 502 804 RH
              GLASS CHAMBER
1976 AUG 16-17
         CLOCK ELAPSED TS1 REL HUM
TIME TIME(MIN) (DEG C) (3)
                                                  50.2
          Z140
                     250.
                                         75.0
                                                 0.250
          2145
                     255.
                               33.9
                                         75.3
                                                 0.247
 (
          2150
                     260.
                               33.8
                                         76.0
                                                 0.244
                                         76.0
                                                 0.244
          Z155
                     265.
                               33.8
          2200
                     270.
                               33.9
                                        75.5
75.5
                                                 0.239
                     275.
                                                 0.247
          2205
                               33.8
          2210
                     2501
                                                 0.243
                               33.7
                                         73.5
 (
          2215
                     285.
                               33.9
                                         75.5
                                                 C.241
          2220
                     290.
                               33.8
                                         75.5
                                                 0.241
          2225
                     255.
                               33.7
                                         75.5
                                                 0.239
 Ć
          2230
                     300.
                               33.9
                                        75.5
                                                 0.239
                                         75.5
          2235
                     305.
                               33.8
                                                 0.235
          2240
                     310.
315.
                               33.7
                                         75.5
                                                 0.236
          2245
                               33.9
                                         75.5
                                                 C.235
          2250
                               33.7
                                         75.5
                     320.
                                                 0.235
2255
                     325.
                               33.7
                                         75.5
          2300
                     330.
                               33.8
                                         75.5
                                                 0.231
          2305
                     335.
                               33.7
                                         75.5
                                                 C.228
          2310
                     340.
                               33.7
                                         75.5
                                                 0.225
                                         75.5
75.5
          2315
                     345.
                               33.7
                                                 0.224
                     350.
                                                 C.221
          2320
                               33.5
          2325
                     355.
                               33.5
                                         75.5
 C
          2330
                     360.
                               33.7
                                         75.5
                                                 0.226
          2335
                     365.
                               33.5
                                         75.5
                                                 C-220
          2340
                     370.
                               33.5
                                         75.3
                                                 0.219
                                         75.5
75.5
 C
          2345
2350
                               33.5
23.4
                                                 0.224
                     375.
                     330.
                     385.
                               33.4
                                         75.5
                                                 C.220
          2355
                               33.5
                                         75.5
                                                 0.213
 Ć
              0
                     390.
                               33.4
                                         75.5
             10
                     400.
                                         75.5
                                                 C.211
             15
                     405.
                               33.4
                                         75.5
                                                 0.213
 C
             20
                     410.
                               33.4
                                         75.5
                                                 C.211
                                         75.5
75.5
                               33.2
33.4
33.2
                     415.
             25
                                                 0.214
                     420.
             30
                                                 0.209
                                         75.5
75.5
                                                 0.214
             35
                     425.
                     430.
                               33.1
                                                  0.211
                     435.
                               33.2
                                         75.5
                                                 0.206
 C
                               33.2
33.1
             50
                     440.
                                         75.5
                                                 C.206
            .55
100
                                         75.5
                                                 0.205
                     445.
                     450.
                                         75.5
                                                 0.204
                               33.2
                                                 C.204
            105
                     455.
                               33.1
                                         75.5
                     46C.
                               33.I
                                         75.5
            110
                     465.
                               33.2
                                         75.5
                                                 0.197
            115
            120
                     47C.
 (
            130
                                         75.5
15.5
                     430.
                               33.1
                                                 0.202
 \Box
            135
                     485.
                               33.0
                                                 0.195
            140
                     450.
455.
                               33.1
33.1
                                                 0.177
                                         75.5
                                         75.5
              ***** NC DATA TAKEN ---- DATA DISCARDED
                                                                            ? QUESTIONABLE CATA
```

```
AGC-219-3 SG2 90% RH
 GLASS CHAMBER
                1976 AUG 17
          CLCCK ELAPSED TS:
TIME TIME(MIN) (DEG C)
                                          REL HUM
                                                      SO2
             150
                        500.
                                   33.1
                                                       C.194
                                             75.5
75.5
75.5
75.5
             155
200
                        505.
510.
                                  33-1
                                                       0-192
                                                      C.191
                                  33.1
             205
                        515.
                                  33.0
             210
                        520.
                                  33.0
                                                       0.192
                        525.
530.
                                  33.1
                                             75.5
75.5
                                                      C.184
             220
                                  32.8
             225
                                                      0.187
 (
                        535.
                                  33.0
                                             75.0
                       540.
                                             75.0
75.5
             230
235
                                                      0.137
                                  23.1
                                  32.8
             24C
                        550.
                                  32.8
                                             75.0
                                                      0.183
             245
250
                        555.
560.
                                  33.0
                                                      0.182
C.180
C.179
                                             75.0
                                             75.0
             255
                        565.
                                  32.8
                                             75.0
             3,00
                        570.
                                   32.8
                                                      0.183
             305
                        575.
                                  32.7
                                             75.0
             310
                        580.
                                  32.7
                                             75.0
                                                      0.176
             315
                       585.
                                  33.0
32.7
                                             75.0
                                                       9.175
             320
                                             75.0
                                                      0.172
įС
             325
                        595.
                                  32.7
32.8
                                             75.0
                                                      0.173
             330
                       600.
                                             75.0
                                                      0.172
             335
                                  32.7
 C
             340
                       610.
                                  32.7
                                             75.0
                                                      0.171
             345
350
                                  32.8
32.7
                       615.
                                             75.0
                       620.
625.
                                             75.0
                                                      0.166
 C
             355
                                  32.7
32.8
32.7
                                             75.0
                                                      0.169
             400
                        630.
                                                      0.165
             405
                                             75.0
             410
                                  32.7
                                             75.0
                                                      0.101
                                  32.8
32.7
             415
420
                       645.
                                             75.0
                                                      0.102
                       650.
                                                       C.160
             425
                       655.
                                  32.7
                                             74.5
                                                      C.158
             430
435
                       665.
                                  32.8
32.7
                                                      C.159
C.159
G.155
                                             74.5
74.5
             443
                       670.
                                  32.7
                                             74.5
                                  32.8
32.7
             445
                                             75.0
74.5
                                                      0.158
0.153
             450
                       680.
             455
                       685.
                                  32.7
                                             74.5
                                                      C.153
             500
                       690.
                                             74.5
74.5
74.5
                                                      C.156
C.150
                                  32.7
32.7
             505
             51C
                       700.
                                  32.7
                                                      0.155
             515
                       705.
                                             74.5
                                  32.7
                                                      C.152
               ***** NO DATA TAKEN
                                                      -- DATA DISCARDED
                                                                                    ? QUESTIONABLE DATA
```

### AGC-219-4 SDZ 808 PH GLASS CHAMBER 1976 AUG 17

# ACD 710 MIN TO ELAPSED TIME

	-	CLCCK TIME.	ELAPSED TIME (MIN)	TSI (DEG C)	REL HUM (%)	SOZ (PPM)		
		520	0.	32.6	74.5	0.149	-	
(		525	5.	32.6	74.5	C.153		
`		530	10.	32.7	74.5	C.147		A CONTRACT OF THE PARTY OF THE
		535	15.	32.6	74.5	C.148		
(		540	20.	32.6	74.5	C.147		
		. 545	25•_	32.7_	74 • 5	0.143		
_		550	30.	32.4	74.5	0-144		
C		555	35.	32.6	74.5	0.143		•
		600	40	32.6	74.5	0.142		
_		605 610	45. 50.	32.4 32.4	74.5 74.5	C.138		
C		615	55.	32.7	74.5			•
		620	60.	32.4	74.5	0.142		
C		625	65.	32.4	74.5	0.136		•
10		630		32.6	74.5	C.134		
• •		635	75.	32.4	74.5	0.133		
-{C		64 C	80.	32.4	74-0	0.136		
į		645	85.	32.4	74.0	0.132		
		650	90.	32.4	74.0	0.131		
C		655	55.	32.4	74.0	0.131		
		700	100.	32.6	74.0	0.131_		
_		705	105.	32.4	74.0	0.127		
C		710	110.	32.4	74.0 74.0	0.128 0.127		
		715 720	115.	32.6		C.126		
_		725	125.	33.0	73.0	0.127		
C		730	130.	33.2	72.5	0.128	*	• •
		735	135.	33.2	72.0	0.121		
C.		740	140-	33.4	72.0	0.125		
~		745	145.	33.5	71.5	0.122		
		750	150.	33.4	71.5	0.121		
Ć		755	155.	33.4	71.5	0.122		•
		800	150.	33.7	71.5	0.122		
٠.		805	165.	. 33.2	72.0	0.121		
C		810		33.1	72.0	0.119		•
		815 820	175. 180.	33.0	72.0 72.0	0.119		
C		825	185.	33.0	72.0	C.119		
· ·		830	190.	33.0	72.0	0.115		
		- 7835	195.	32.8	72.0	0.120		
C		840		32.8	72.0	0.112		
•		845	205-	32.8	72.0	0.119		The second secon
		850		32.8	72.0	0.112		•
C		855		32.8	72-0	0.114		
		930		33.0		0.110		والمراج المحمد ومراج والمراكز والمراج والمستنصب بميسي يماسون
42		905	225.	32.8	72.0	0.112	•	
C								•
ė								•
(								· ·
۲.								•
		910	230.	32.8	72.0	C.109		
C		915		32.8	73.0	0.108		
~		920		32.7	73.5	C.153		
		925		32.7	73.5	0.109		
C								
			***** NO E	DATA TAKE	N -	DATA	DISCAPDED	7 QUESTIONABLE DATA

AGC-219-5 SO2 806 RH GLASS CHAMBER 1976 AUG 17

ADD 710 MIN TO ELAPSED TINE

											.•					
	CLOCK TIME	ELAPSED TIME(MIN)	TS1 : I	REL HUM	SO2 (PPM)											
			1000 07	, .,	******											
	930	250.	32.5	74.0	0.103		• •				· -:					
•	935 940	255. 260.	32.7	74.0	0.104		•									
4.	945	265.	32.8	74.0	0.106								-			
	950 955	270. 275.	32.7	73.5 73.0	0.108									-		
	1000	280.	32.7		0.106				· - · <del>- · · · · · · · · · · · · · · · ·</del>							
	*1	**** NO D	ATA TAKEN		CATA	DISC	ARDED .		QUEST	IONABLI	DATA.				-	
										٠.						
					•											
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		• • • •					<del></del> -			<del>, , , , , , , , , , , , , , , , , , , </del>				· · · · · · ·		
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		·						<del></del> .								-
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٠.												<u> </u>			-	
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			ti de martin de martin de la composição de		<del></del>						<del> </del>					
	-										•					

AGC-220-1 SO2-03 PROPENE GLASS CHAMBER 1976 AUG 19

DARK 502 AND FC-12 INJECTED AT 1115 OZONE ADDED AT 1149, PROPENE AT 1155 BRADY 1296, CALIBRATION 1976 JULY 16

```
CLCCK
               ELAPSED
                           DZONE
                                      TS1
                                            REL HUM
                                                        $02
                                                               PROPENS
              TIMEIMINE
                           (PPH)
                                   1086 C1
                                             (T)
                                                       (PPH)
                                                                (PPM)
         1200
                     С.
                           0.654
                                               41.0
                                                       0.363
                                                                1.014
         1205
                     5.
                           0.606
                                      32.8
                                               41.0
                                                       0.344
         1211
                    11.
                           0.557
                                     32.8
32.8
                                               41.0
                                                       0.331
                                                               *****
         1216
                    16.
                           0.511
                                               41.0
                                                       0.318
                                                                0.801
         1221
                    21.
                           0.474
                                      32.7
                                               41.0
                                                       0.304
                                                               ***
         1226
                    26.
                           0.440
                                      32.7
                                                               ****
                                               41.0
                                                       0.297
         1230
                    30.
                                      32.8
                                               41.0
                                                       0.291
                                                                0.683
         1235
                    35.
                           0.393
                                      32.7
                                                       0.283
         1240
                           0.371
                    40.
                                      32.8
         1245
                    45.
                           0.352
                                      32.8
                                               41.0
                                                       0.271
                                                                0.593
         1250
                    50.
                           0.335
                                      32.8
                                               41.0
                                                       0.266
                                                               表示表示故意
         1255
                    55.
                           0.318
                                      33.0
                                                               ****
                                               40.5
                                                       0.246
         1300
                    60.
                           0.303
                                               40.5
                                                       0.260
                                                               0.522
\overline{\phantom{a}}
         1305
                    65.
                           0.286
                                      32.8
                                               40.5
                                                       0.258
         1310
                    70.
                           0.274
                                      32.8
                                               40.5
                                                       0.254
                                                               ****
                    75.
         1315
                           0.259
                                      32.3
                                               40.5
                                                       0.250
                                                               ****
         1320
                    80.
                           0.249
                                      32.8
                                               40.5
                                                       0.249
                                                               ****
         1325
                    85.
                           0.239
                                     32.8
                                               40.5
                                                               ****
                                                       0.249
         133,1
                    91.
                           0.230
                                     32.6
                                               40.0
                                                                0.434
                                                       0.247
Ç
         1336
                    œ.
                           0.222
                                     32.8
                                               40.0
                                                       0.244
         1341
                   101.
                           0.213
                                      32.8
                                               40.0
                                                               ** ** *
                                                       0.242
         1346
                   105.
                           0.205
                                      32.8
                                               40.0
                                                       0.238
                                                               ****
         1350
                   110.
                           0.200
                                     32.8
                                               40.0
                                                       0.239
                                                               ****
         1355
                                     32.8
33.0
                           0.191
                                                               ****
                                               40.0
                                                       0.239
         1400
                   120.
                           0.136
                                                       0.237
                                                                0.376
(
         1405
                   125.
                           0.178
                                     32.8
                                               39.5
         1410
                   130.
                           0.176
                                      32.8
                                                       0.233
                                                               ****
         1415
                   135.
                           0.156
                                     32.8
                                               39.5
                                                       0.231
                                                               ** ** **
         1420
                   140.
                           0.151
                                     32.8
                                               39.5
                                                               *****
                                                       0.232
         1425
                   145.
                           0.159
                                     32.8
                                               39.5
                                                               ****
                                                       0.230
         1430
                   150.
                           0.151
                                     32.8
                                               39.5
                                                       0.230
                                                                0.336
        1435
                   155.
                           0.147
                                     33.0
                                               39.5
                                                       0.226
        1440
                   160.
                           0.142
                                     32.8
                                               39.5
         1445
                   165.
                           0.139
                                     33.0
                                               39.5
                                                       0.225
                                                               ****
         1451
                   171.
                           0.134
                                     32.8
                                               34.5
                                                               ****
                                                       0.223
         1456
                   176.
                           0.132
                                               39.5
                                     32.8
                                                       0.223
         1501
                   181.
                           0.127
                                     32.8
                                               39.0
                                                       0.222
                                                                0.311
         1506
                   186.
                           0.122
                                     32.8
                                               39.0
         1510
                   190.
                           0.122
                                     33.0
                                               39.0
                                                       0.221
                                                               ****
                   195.
                           0.120
                                     32.8
                                               39.0
                                                       0.221
                                                               力ながおかね
         1520
                   200.
                           0.115
                                     32.8
                                               39.0
                                                               *****
                                                       0.220
         1525
                   205.
                           0.110
                                     32.8
                                               39.0
                                                       0.220
                   219.
215.
220.
        1530
1535
                           Ç.110
                                     33.0
                                               39.0
                                                       0.221
                                                                0.289
                          0.105
                                     32.8
                                               39.0
                                                       0.216
         1540
                                     32.8
                                               39.0
                                                       0.216
                                                               *****
         1545
                                     32.8
                                               39.0
                                                       0.215
                                                               ****
        1550
1555
                   236.
235.
                                     32.8
33.0
                                              39.0
39.0
                                                      0.215
                                                               ****
                         *****
                                                               ****
        1600
                   240.
                          ******
                                     33.0
                                               39.0
                                                       0.213
                                                                0.274
        1605
                   245.
                           0.088
                                     32.8
                                               39.0
                    NO DATA TAKEN
                                          ---- DATA DISCARDED
                                                                       7 QUESTIONABLE DATA
```

AGC-220-2 SD2-D3 PROPENE GLASS CHAMBER 1976 AUG 19

	CLCCK		OZONE	TS1	REL HUM	502	PROPENE (PPM)		
	TIME	TIME (MIN)	(PP4)	(DEG C)	(3)	(ppy)	( PPF F I		
(									
				20.0	38.5	0.214	****		
	1611	251.	0.085	33.0	38.5	0.211	*****		
	1616		0.090	32.8	38.5	0.211	****	•	
	1621		0.085	33.0	38.5	0.228	****		•
	1626		0.083	33.0		0.208	0.254		
	1630		0.083	33.0	33.5		<b>0.∠</b> 24		
	1635		0.031	33.0	32.5	0.208			
	1640		0.078	33.0	33.5	0.209	*****		
	1645	285.	0.076	33.1	38.5	0.205	****		
•,	1650	290.	0.076		38.5	0.205	****		•
	1655	295.	0.076	33.0	38.5	0.206	****		
( ·	1700	300.	0.071	33.8	38.5	C.205	0.248		
. ~	•					_ = = = = = = = = = = = = = = = = = = =			DATA
	*	**** NO D	ATA TAKE	EN -	DATA	DISCAR	350	? QUESTIONABLE	LAIA
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AGC-221-1 SO2-03 GLASS CHAMBER 1976 AUG 20

DARK BRADY 1296, CALIBRATION 1976 JULY 16 OZDNE WAS INJECTED AT 0933

CLOCK TIME	FLAFSED TIME (MIN)	020NE (M94)	TSI (DEG C)	REL HUM	SC2 (PP#)
845 850 855 900 915 915 925 930 946 951 1020 1025 1010 1025 1010 1035 1040 1055 1100 1111 1116 1125 1130 1135 1145 1150 1121 1120 1215 1220 1226 1231	71   (MIN)  0. 5. 10. 25. 30. 25. 30. 49. 50. 55. 61. 66. 71. 75. 80. 85. 105. 110. 115. 120. 135. 141. 146. 151. 155. 160. 185. 170. 185. 190. 205. 215. 221. 226.				
1236 1240 1245	231. 235. 240.	0.503 0.501 0.501	33.0 33.0 33.0	40.5 40.5 40.0	0.319 0.318 0.315

***** NO DATA TAKEN

---- DATA DISCAPDED

7 QUESTIONABLE DATA

AGC-221-2 SD2-03 GLASS CHAMBER 1976 AUG 20

_	FINC V	ELAPSED	0.7005				
		TIME (MIN)	OZONE	TSI	REL HUN	205	to any control of the state of
	4 L ME	* TWC FWTN1	(PPM)	(DEG C)	(%)	(PPM)	
				•			
	1255	250.	0.498	33.0	4C.0		
	1300	255.	0.493	33.1	40.0	0.313	
	1305	260.	0.493	33.0	40.0	0.309	
	1310	265.	0.491	33.0	39.5	0.308	
	1315	270.	0.491	33.2	39.5	0.308	
	1320	275.	0.489	33.1	39.5	0.310	
	1325	280.	0.489	33.1	39.C	0.309	The same and the s
	1330	285.	0.484	33.2	39. C	0.307	
	1335	290.	0.484	33.2	39.C	0.308	
	1340	295.	0.481	33.2	39.0	0.304	and the state of t
	1346	301-	0.481	33.2	38.5	0.303	
	1351	306.	0.479	33.2	39. C	0.304	
	1356	311.	0.479	33.1	39.0	0.303	and the constraints of the second sec
	1400	315.	0.476	33.1	39.0	0.302	
	1405	320.	0.476	33.1	39.0	0.299	
	1410	325.	0.474	33.1	39.0		
	1415	330.	0.474	33.1	38.5	0.298 0.298	
	1420	335.	0.471	33.1	38.5	0.296	
	1425	340.	0.469	33.1	38.5	0.294	The residual management of the contract of the
	1430	345.	0.467	33.2	38.5	0.296	
						0.270	
							•
	**	**** NO DA	TA TAKE	<u> </u>	DATA	DISCARDED	2 GIESTIONARIE DATA
	**	**** NO DA	TA TAKE	4	DATA	DISCARDED	? QUESTIONABLE DATA
	**	**** NO DA	ITA TAKE		DATA	DISCARDED	
	**	**** NO DA	TA TAKE	-	DATA	DISCARDED	? QUESTIONABLE DATA
	**	**** NO DA	TA TAKE		DATA	DISCARDED	
	**	**** NO DA	ITA TAKE		DATA	DISCARDED	
	**	**** NO DA	TA TAKE	-	- DATA	DISCARDED	
	**	**** NO DA	TA TAKE		DATA	DISCARDED	
	**	**** NO DA	TA TAKE	\	DATA	DISCARDED	
	**	**** NO DA	TA TAKE	-	DATA	DISCARDED	
	**	**** NO DA	TA TAKE		DATA	DISCARDED	
	**	**** NO DA	TA TAKE	· · · · · · · · · · · · · · · · · · ·	— DATA	DISCARDED	
	**	**** NO DA	TA TAKE	1	DATA	DISCARDED	
	**	**** NO DA	TA TAKE		— DATA	DISCARDED	
	**	**** NO DA	TA TAKE		— DATA	DISCARDED	
	**	**** NO DA	TA TAKS		— DATA	DISCARDED	
	**	**** NO DA	TA TAKE		DATA	DISCARDED	
	**	**** NO DA	TA TAKE		DATA	DISCARDED	
	**	**** NO DA	TA TAKS		— DATA	DISCARDED	
	**	**** NO DA	TA TAKE		DATA	DISCARDED	

AGC-222+1 SU2-NOX-SURR-U GEASS CHAMBER 1976 AUG 24

[]

DARK
CO FACTOR 1.9/1.22: BRADY 1295
2.1 ML NOX INJECTED AT 0920 HJURS
AT T=0: NON-METHANE MC = 1740 PPSC; METHANE = 3200 PPB

•	TIPE	TIME (MIN)	(PPM)	(PPM)	(DEG C)	(2)	( PP M )
•							
	945			5.63	33.2	46.5	0.349
	950		0.0	5.60	33.1	46.5	0.348
	955		0.002	5.65	33.1	45.5	0.344
	1000		0.0	5.01	33.0	46.5	0.344
	1005	20.	0.0	5.60	33.0	46.5	0.340
	_ 1010	25.	****	*****	*****	*****	****
	1015		0.0	5.63	33.0	46.5	0.338
	1020	35.	0.0	5.64	33.0	46.5	0.338
			0.0	5.58	33.0	46.5	0.337
	1030		0.0	5.56	33.0	46.5	0.333
	1035	50.	0.0	5.56	33.0	46.5	
	1045	<del>55.</del>		5.56	33.0	46.0	0.33Z
	1050		0.0	5.51	33.0	45.0	0.332
	1055	65. 70.		5.52	33.0	46.0	0.333
	1100	75.	0.0	5.48	33.0	46.0	0.329
	1105	80.	0.0	5.48	33.0	45.5	0.329
	1110	85.	0.0	5.48	33.0	45.5	0.327
	-1115	90.	0.0	5.47	33.1	42.2	0.340
	1120	90. 95.	0.0	5.50	33.1	45.5	0.326
	1125	100.	0.0	5.48	33.1	45.5	
	1130	105.	0.002	5.45 5.42	33.1	45.5	0.324
	1135	110.	0.002	5.40		45-0	0.322
	1140	115.	0.002	5.42	33.0 33.0	45.0	0.319
	1145	120.	0.002	5.38	33.0	45.0 45.0	0.320
	1150	125.	0.0	5.40	33.0	45.0	0.319
	1156	131.	0.0	5.41	33.0	45.0	0.318
	1200	135.	0.C	5.32	33.0	45.C	0.318
	1205	140.	0.010	5.39	33.0	45.0	0.314 0.311 .
	1210	145.	0.0	5.35	33.0	45.0	0.314
	1215	150.	0.0	5.34	32.8	45.0	0.313
	1220	155.	0.0	5.33	33.0	44.5	0.310
_	1225	160.	0.0	5.34	33.0	44.5	0.313
	1230	165.	0.0	5.26	33.0	44.5	0.313
	1235	170.	0.0	5.31	33.0	44.5	0.310
	1240	175.	0.0	5.30	33.2	44.C	0.308
	1245	180.	0.0	5.26	33.1	44.0	0.308
	1250	185.	0.0	5.28	33.2	44 - C	0.307
•	1255_	190	0.0	5- 29	33.2	43.5	0.304
	1300	195.	0.0	5.23	33.2	43.5	0.305
	1305	200.	0.0	5.26	33.2	43.5	0.304
	1310	205.	0.0	5.24_	33.2	43.5	0.304
	1315	210.	0.002	5.24	23.2	43.5	0.302
	1320	215.	0.0	5.23	33.2	43.5	0.300
	1325	220•	_0.0	5.18	33.2	43.C	0.300
	1330	225.	0.0	5.19	33.2	43.0	0.305

					-		
_	1335	230.	0.0	5.19	33.2	43.6	0.300
[ [ ]	1341	236.	0.002	5.16	33.1	43.0	3.277
	1345	240.	0.0	5.15	33.1	43.0	3.297
	1350	245.	0.0	5.13	33.2	43.5	0.236

***** NO 54TA TAKEN

--- DATA DISCAPDED

? QUESTIONABLE DATA

AGC-222-2 502-NOX-SURR-U GLASS CHAMBER 1976 AUG 24 CLOCK ELAPSED TIME TIME(MIN) DZONE (PPM) CO (PPM) TS1 REL HI HUN 33.2 0.296 1355 250. 0.0 5.13 43.C 1400 255. 0.0 5.12 33.2 43.C 0.294 ( 1405 260. 0.0 33.2 43<u>.</u> C 0.293 1410 265. 0.0 5.12 33.0 43.0 0.291 5.00 33.0 43.0 1415 270. 0.0 0.291 275. 5.07 32.8 32.8 0.0 43.0 1420 43.C 0.291 280. 1425 285. 0.0 5.78 32.8 42.5 0.291 1430 C 0.291 1435 1440 290. 0.0 5-04 32.8 42.5 0.289 42.5 1445 300. C.0 5.02 33.0 0.283 C 5.02 4.97 42.5 42.0 0.288 1450 305. 0.0 33.0 33.0 1455 310. 0.0 0.0 4.99 33.0 42.C 0.285 C Distance Com. 1500 315. 1505 4.96 33.0 42.C 0.285 320. 0.0 1510 325. 0.0 5.00 42.0 0.285 1515 330. 0.0 5.01 33.0 42.C 0.285 4.93 4.96 33.0 33.1 41.5 1520 335. 0.002 0.282 4 341. 0.281 1526 0.0 ₃€ 41.5 33.4 0.280 4.93 1530 345. 0.0 350. 355. 4.92 33.2 33.1 41.5 41.5 0.280 1535 1540 0.0 4.91 0.002 C 1545 0.002 4.92 33.0 41.5 0.280 360. 1550 365. 6.0 4.93 32.8 41.5 0.276 41.5 41.5 1555 370. 0.0 4.89 32.8 C 0.275 1600 375. 0.0 4.89 32.8 0.271 4.88 4.90 33.0 32.8 41.5 1610 380. 0.0 385. 41.0 0.002 0.274 1615 0.002 4.83 33.0 41.0 0.272 390. 4.87 41.0 0.271 1620 395. 0.0 33.0 1625 4.81 33.0 41.0 0.274 C 41.0 1630 405. 0.002 4.81 33.0 0.270 33.0 33.0 41.6 0.273 1635 410. 0.002 4.87 0.270 1640 415. 0.0 4.80 €. 0.002 4.85 33.0 4C.5 0.269 1645 420. 425. 0.270 1650 0.002 4-81 33.0 40.5 1655 430. 0.0 4.83 33.0 40.5 0.266 1700 435. 0.0 4.84 33.0 40.5 0.265 33.0 33.1 1705 440. 4-82 40.5 0.266 Ĩ71Ï 40.5 446. 0.0 4.82 0.266 4.77 4.74 4.79 40.C 33.2 0.264 450. 1715 0.0 1720 33.2 40.0 0.264 455. 0.0 33.2 0.265 1725 460. 0.0 40. C 465. 0.0 4.79 33.2 40.C 0.265 1730 0.0 1735 470. 4.80 33.1 40.0 0.264 1740 475. 33.2 40.0 0.265 ( 33.2 33.2 33.2 40.C 40.C 40.C 0.0 1745 480. 4.80 0.265 1750 1755 485. 4.77 4.72 4.72 0.261 490. 0.0 0.260

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33.1

0.260

7 QUESTIONABLE GATA

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		··						
cro	C.K.	ELAPSEC	DZCNE	co	T51	REL HUM	: 502	
TIH	=	TIME (MIN)	(PPM)	(PPM)	LDEG CI	(3)	(PPM)	
								•
180	oʻs —	500.	0.0	4.72	33.1			
181	lo	505.	0.0	4.72	33.2	39.5	0.261	
181	15_	510.	0.0	4.70	33.9	39.5 39.5	0.256	•
182		515.	0.0	4.69	34.1	39.5	0.259 0.256	ر المحمد
182		520.	0.0	4.69	34.1	39.5	0.256	•
183		525.	0.0	4.68	34.1	39.5	0.255	$\epsilon_{ij}$
183		530.	0.0	4.67	34.1	39.5	0.256	
184		535.	0.0	4.66	34.2	39.5	0.254	
184		540.	0.0	4.69	34.2	39.5	0.254	•
189		545.	0.0	4.67	34.2	39.5	0.253	
190		551.	0.0	4-66	34.3	39.5	0.255	
190		555. 560.	0.0	4.66	34.1	39.5	0.254	
191		565.	0.0	4.70	34.1	39.5	0.254	
191		570.	0.0	4.65	34.1	39.5	0.252	
192		575.	0.0	4.64	34.1	39.5	0.252	
192		580.	0.0	4.58	34.1 34.1	39.5	0.249	
193	0	585.	0.0	4.58	34.1	39.0 39.0	0.249	
193		590.	0.0	4.65	34.1	39.5	0.247	
194		595.	0.0	4.60	33.9	39.0	0.245	
194	5	600.	0.0	4.58	33.9	39.0	0.245	
195		605.	0.0	4.58	34.1	39.0	0.247	
195		61C.	0.0	4.61	33.8	39.0	0.244	
200		615.	0.0	4.60	33.8	39.0	0.245	•
201		620.	0.0	4.56	33.9	39.C	0.244	
201		625. 630.	0.002	4.54	33.9	39.0	0.245	
202		635.	0.0	4.59	33.9	39.C	0.243	
202		640.	0.002	4.56 4.53	33.9	39.C	0.245	
203		645.	0.0	4.55	33.9 33.9	39.0	0.241	
203		650.	0.0	4.58	33.9	39.0	0.241	
204		656.	0.002	4.59	33.9	39.0 39.0	0.239	The state of the s
204		660.	0.002	4.59	33.8	38.5	0.239 _0.238	•
2050			0.002	4.52	33.8	38.5	0.237	
2055		670.	0.0	4.51.	33.9	38.5	0.237	<del></del>
2100			0.0	4-51	33.9	38.5	0.237	
2109			0.0	4.48	33.9	38.5	0.237	
2110			0.0	4.53	33.9	38.5	0.236	•
2120			0.0	4.48	33.9	38.5	0.236	
2125			0.0	4.49	33.9	38.5	0.236	
2130			0.0 0.0	4-55	33.9	33.5	0.232	
			Y	4.49	33.9	38.5	0.234	

#### AGC-222-4 SC2-NOX-SURR-U GLASS CHAMCER 1976 AUG 24-25

ADD 710 MIN TO ELAPSED TIME

	.APSED (F(#14)	DZCNE {PPM}	(228) ····	751 (366-01)	REL MEN	(85 <b>%)</b> 200
2135	c.	0.0	4.49	23.9	38.5	3.232
- 2140	5.	3.0	4.5i	3.8	33.5	U-222
2145	16-	0.0	4.49	23.8	33.	0.231
215C	15.	0.0	4+48	33.9	30.5	0.231
2155	2¢.	0.0	4.45	23.9	38.5	0.231
2200	25.	0.0	4,45	33.5	38.5 ⋅	0.226
2205	30.	0.0	4.45	33.8	38.5	0.228
2210	35.	ē.c	4.40	33.9	35.9	3.227
2215	40.	0.0	4.41	33.8	38.0	0.228
5350	45.	0.0	7.45	33.6	39.5	0.270
7226	51.		4.45	33.8	365	0.227
2220		0.0	4 + 45 4 + 45		38.5	0.230
2230	55.	0.0		33.7		
2235	ۂ.	0.0		33.7	3 3 . 5	0.225
2240	ć5.	0.0	4,40	33.7	39.5	0.225
2245	70.	0.0	4.37	33.8	38.5	3.226
2250	75.	0.0	4.40		35.5	0.223
2255	80.	0.0	4.43	33.5	36.5	0.223
2300	₹5.	0.0	4.43	33.5	33.5	0.222
2305	9C.	0.5	4.40	33.5	38.5	0.222
2310	95.	0.0	4.40	33.4	3₫.5	0.221
2315	100.	0.0	4.39	23.4	33.5	0.221
2320	105.	0.0	4,39	23.4 23.4	38.5	C.221
2325	110.	0.0	4.40	33.2	38.5	6.232
2330	115.	0.0	4.41	33.2	38.5	0.221
2335	120.	0.0		33.2	38.5	0.225
2340	125.	0.0	4.34	33.2	38.5	0.223
2340	125.			33.2		0.222
2345	130. 135.	0.0	4-33	23 - 4	38.5	0.219
2350	1 3 5 .		4.34	33.1	33.5	
2355	140.	0.0	4.35	33.1	38.5	0.217
C	145.	0.0	4.32	33.1	3,5 . 5	0.219
5	150.	0 - 0	4.31	33.1	33.5	0.220
11	156.	0.0	4.27	0 ، د 3	38.5	0.216
15	100.	C.C	4.27	32.8	:39 <b>.</b> C	3.216
20	165.	0.0	4.24	32.8	39.0	0.216
25	170.	0.0	4.24	32.8	39.0	0.215
30	175.	0.0	4.33	33,C	39.0	0.215
35	1:0.	0.0	4.24	32.8	39.0	0.214
4 C	185.	0.0	4.29	32.€	39.0	0.217
45	120.	0.0	4.25	32.8	39.0	C.213
50	135.	0.0	4.31	32.6	3 0	0.213
-55	200.	0.0	4.25	32.€	39.0	0.211
100	205.	0.0	4.27	32.8	3 9 . C	0.214
105	210.	0.0	4.27	32.1	35.0	3.211
110	215.	0.0	4.26	32.6	39.0	0.211
			4.25	32.0	35.0	0.209
115	22C•	0.0	4.23	32.7	39.0	0.213
120	225.	0.0	* ** € 3	32.4	29.6	0.213
6 × 100 × 10 × 10				•		
					*	
125	230.	0.C	4.22	32.7	39.0	6.269
130	234	0.0	4.21	32.7	39.0	3.213
135 .	340.	0.0	. 9.29	22.7	33.4	0.215
140	245.	υ•C	4.25	32.7	35.0	0.208
1.40	245.	U + C	77 <b>≠</b> 2.37	ا به عند		3 4 E W ()

***** 10 DATA TAKEL

? CUESTIONABLE LATA

## AGC-202-5 SCC-NCX-SURR-U GLASS CHAMBER 1976 AUG 25

## ACD 710 MIN TO ELAPSED TIME

 $\Box$ 

LIME	ELAPSED TIME(MIN)	CZONE.	CC (PPH)	181 (Dec 2)	REL HU"	\$02 (PPM)
	1102(021)	*******	4: • .,,		101	( ) ( ) ( ) ( )
145	Z5C.	0.0	4.15	32.A	39.0	0.200
150	255.	0.0	4.21	32.6	39.0	0.504
156	261.	Ǖ0	4 - 21	32.5	35.0	0.208
200	265.	0.0	4.19	32.4	35.0	0.205
205		0.0	4.22	32.3	39.C	0.204
210	275. ' 280.	0.0	4.23	32.•4	39.€ 39.€	0.202
220			4.16	32.4		0.204
225	290.	0.0 0.3	4.19	32.3	35.0 35.5	0.205
230	295.	- 0.0 0.0	4.17	32.3	39.5	0.205 د200
235		0.0	4.16	32.3	34.5	0.50:
240		c.c	4.10	32.3	35.5	0.202
245		0.0	4.21	32.3	39.5	0.202
250		0.0	4.16	31.5	35.5	0.200
255		2.0	4.11	31.6	35.5	0.202
330		0.0	4.07	31.5	35.5	6.202
305		0.0	4.14	31.43	35.5	0.200
310		0.0	4.10		35.5	0.202
315	340.	C.C	4.13	31.3	39.5	0.200
320		0.0	4.14	31.3	39.5	0.260
325	350.	0.0	4.39	31.3	39.5	0.196
330		C.C	4.10	31.2	35.5	0.197
335	360.	0.0	4.10	31.2	35.5	0.196
341	366.	0.0	4.54	31.2	35.5	0.197
345		0.0	4.08	31.2	35.5	0.197
350		0.0	4.38	31.2	39.5	0.195
3 5 5		0.3	4.01	31.2	35.5	C.195
400		0.0	4.02	31.2	35.5	0.195
405		0.0	4.ča	31.1	33.5	د155 د
41 C		0.0	4.04	31.2	35.5	0.197
415		0-0	4.07	31.1	35.5	0.152
420		0.0	4.04	31.1	39.5	0.192
425		(.• ç	4.32	31.1	33.5	0.192
430		0.0	3.99 4.27	31.1	35.5 31.5	0.193
440		<u>0.5</u>	4.52	31.1 31.i	37.5	0.191
445		5.0	3.98	31.1	35.5	0.189
450		0.0	3.93	31.1	37.5	0.189
455		0.0	4.22	31.1	37.5	3.189
500		0.0	4-01	- 30.€	35.5	0.196
505		0.0	4.50	30.9	39.5	0.188
510			3.55	30.9	3 , , 5	5.185
515		0.0	3.93	30.9	31.5	0.197
520		0. C	3.57	30.8	31.5	0.180
526	571.	_0.0	3.55	30.8	35.5	J.187
530	475.	0.0	4.01	30.8	37.5	0.186
		*** **				
*						
	1000 m		err comment			
535 540		0.0 0.0	3.97	30.8	37.5	0.1d7
545		2.0	4.20 3.99	30.3 30.7	يئيو≸ ئاين∂ق	3.154
550		5.0	3.98	30.7 30.8	3 3 5	€ . 1 d ¢ U . 1 84
,,,,	7724	J • U	3.70	30.5	3 1 + 3	U . L

. .. ---- CATA DISCAPDEC

AGC-222-6 SO2-NOX-SURR-U GLASS CHAMBER 1976 AUG 25

ADD 710 MIN TO ELAPSED TIME

		ELAPSED TIME(MIN)	0Z0NE (99%)	(C) (E24)	TS1 (DEG C)	R71 HER 141	\$32 (454)	·
	1130	1 200, 4772141		• • • • • • • • • • • • • • • • • • • •	1320 01			•
	555	500.	0.0	2.93	30.7	29.5	0.134	
	600	505.	<b>3.</b> 0	3.93	30.7	39.5	3.132	
	605	510.	0.0	5.95	30.7	34.5	0.163	
***	610	515.	0.0	3.48	30.7	37.5	3.152	
	615	520.	0.0	3.96	30.7	37.5	0.163	
	620	525.	0.0	3.97	30.7	39.5	0.184	•
·	625	530.	0.0	3.92	30.7	33.5	0.150	
	630	535.	0.C	3.89	30.7	34.5	0.130	
	635	545.	3.0	3, 95	30.7	ط و ز د	3.181	
	640	545.	5.032	3.92	30.7	· 39.5 ·	5.173	
	645	550.	0.002	3.91	30.5	39.5	3.131	
				3.03	30.5	39.5	3.173	
	650		0.0					
	655	560.	0.0	3.95	30.5	37.5	3.177	
	. 730	565.	0.0	3.39	30.5	39.5	3.177	
	705	570.	0.0	3.91	30.7	33.5	7.170	
	711	576.	T 6:0	3.91	30.5	39.5	5.177	•
	715	580.	0.002 .	3.85	30.5	37.5	3.176	
	720	535.	0.0	3.80	30.5	39.0	0.173	
	725	550.	0.0	5.91	30.5	39.0	3.177	Committee and the committee of the commi
	73.0	593.	0.002	3.85	30.5	39.C	J.176	
	735	600.	500.0	3.82	30.5	39.0	0.176	•
*****	740		0.002	3.37	30.5	39.0	3.176	and and the second of the control of
	745		0.0	3.81	30.5	30.0	3.173	
	750	615.	0.0	3.81	33.9	3:40	3.172	
	755		0.002	3.83	31.2	در آه	5.172	conservation of the conser
					31.3	37.0	3.172	
	800	625.	0.0	3.81				
	805		0.002	3.34		37+C_	J.172	and an arms of the second second
	810		0.0	3.83	31.8	35.5	3.172	•
	815		<b>0.</b> 0	3.35	32.0	34.0	1.173	
	820	645.	3.0	3.32	32.0	25.0	0.172	
	925	650.	0.0	3.31	32.3	35.5	0.171	
	830	655.	0.0	3.86	32.3	35.5	5.173	
	835	660.	0.0	3.77	32.3	35.0	1.170	
14-1	340		6.5	3.30	32.4	35.0	.167	and the second s
	845		0.0	3.78		34.5	3.171	•
	850		0.0	3.86	32.7	34.5	0.159	
***	856		0.0	3.30	32.7	37.6	5.157	and the second s
	900		0.0	3.73	32.3	3+.0	3.157	
				3.78		34.0	5.169	
	905		~ Č • Š	at the same	32			
	910	. 695.	0.0	3.84	32.3	31.0	1.169	
		***** NO D	ATA TAKE		CATA	DISCARUS	E 10	P OUESTIONABLE LATA

AGC-222-7 SO2-NOX-SURR-U GLASS CHAMBER 1976 AUG 25

#### ADD 710 MIN TO ELAPSED TIME

CLOCK TIME	ELAPSED TIME("IN)	0Z018 (PPM)	CD (PRM)	TS1 (DEG C)	RSE HUM (%)	\$32 (PP#)	· · · · · · · · ·			 	
915	7252		3.79	32.7	34.0	0.167				 	
920	165.	0.002	3.77	32.7	34.0	0.169					
925	710.	5.0	3.79	32.7	34.0	0.165					
930	715.	0.0	3.79	32.7	33.5	0.162	1				
935	720.	0.0	5.77	32.7	33.5	0.164					
940	725.	0.0	3.77	32.8	33.5	0.162					
945	733.	0.0	3.79	32.3	33.5	C.164				 	
950	735.	0.0	3.73	32.3	33.0	0.162					
955	740.	0.0	3.79	32.8	33.0	0.154					
1000	745.	0.0	3.75	33.5	33.0	0.162					
1005	750.	0.0	3.75	33.8	33.0	0.162					
1010	755.	0.0	3.76	33.S	.33.0	0.161					
1015	1:0.	0.0	3.72	33. €	32.5	0.1=0				 	
1020	7:5.	0.0	3.73	33.9	32.5	0.161					
1025	770.	0.0	3.75	35.9	32.5	0.159					
1030	775.	C.O .	3.78	33.8	32.5	0.159				 	
1035	780.	0.002	3.75	33.8	32.5	0.153					
1041	755.	0.0	3.75	33.3	32.5	0.161					
1045	740.	C.0	3.75	33.7	32.5	C.158				 	
1050	755.	0.0	3.76	33.7	32.5	0.158					
1055	8.0.	0.0	3.75	33.6	32.5	0.156				 	
*	***** 1.3 0/	ATA TAKE	N -	ATA0	DISCARDE	:0	? QUEST	IONABLE	DATA		
				***************************************			a material description of the factor	h des Brette h ette			•

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7466-222-8 302-NOX-SURK-U
 GLASS CHAMBER
             1976 AUG 25
     TUIGHTS ON 1100; INTENSITY 1001
       CO FACTOR 1.9/1.22; BRACY 1296
       TECO 140 WAS ON THE CHAMBER FROM 1105 TO 1111, 1200 TO 1205, 1300 TO 1305, 1400
         "TO" 1405; 1500 TC 1505; 1605 TO 1610; AND 1655 TO 1700
       TECO 140 SAMPLING RATE: 1128 ML/MIN
       PAN NOT MEASURED: NOZ AND NOX VALUES NOT CORRECTED
       "AT T=15 MIN: NON-METHANE HC ="1130 PP8C;" METHANE ="2963 PP8"
        CLOCK ELAPSED DZONE NO NOZE-PAN NOXE-PAN CO TSI REL HUM 502
TIME TIME(MIN) (PPN) (PPN) (PPN) (PPN) (PPN) (DEC C) (X) (PPN)
          1100
                                   FFRLES.
                                            *****
                                                    ******
                           5.0
                     5.
          1105
                           0.027
                                   ****
                                            ****
                                                     *****
                                                                3.74
                                                                                 32.0
                                                                                         0.154
          1110
                    10.
                                    0.030
                                             0.500
                                                      0.530
                           0.054
                                                                3.74
                                                                         34.1
                                                                                 31.5
                                                                                         0.153
                           0.376
                                   ****
          1115
                                                     ****
                     15.
                                                                3.75
                                                                        34.3
                                                                                 37.0
                                                                                         0.149
          1123
                     20.
                                            *****
                                                     *****
                           0.095
                                                                3.73
                                                                         34.3
                                                                                 32.5
                                                                                         0.149
          1125
                                   ****
                                                     *****
                     25.
                           0.110
                                                                3.73
                                                                         34.1
                                                                                 32.5
                                                                                         0.148
                           0.122
                                   ******
                                            *****
                                                     *****
                                                                                         0.145
          1130
                                                                         34.1
                                                                3.73
                                   ****
          1135
                     35.
                           0.132
                                                                         34.1
                                                                                 32.5
                                                                3.70
                                                                                         0.145
          1140
                     40.
                                   ****
                                            *****
                                                     ****
                           0.142
                                                                3.73
                                                                         34.1
                                                                                         0-147
          1145
                    45.
                           0.154
                                   ***
                                            *****
                                                     *****
          1150
                                                                                 32.0
                    5C.
                           0.164
                                   ****
                                            *****
                                                     *****
                                                                3.73
                                                                         34.3
                                                                                         0.143
                                   ***
          1155
                                            ****
                     55.
                           0.176
                                                     *****
                                                                3.73
                                                                        33.4
                                                                                 31.5
                                                                                         0.143
          IZCO
                                            *****
                                                     448224
                    60.
                           J. 131
                                                                         33.5
                                                                3-77
                                                                                 31.5
                                                                                         0.144
          1205
                    65.
                           0.138
                                    0.021
                                             0.443
                                                     0.468
                                                                         33.5
                                                                3.71
                                                                                 31.5
                                                                                         0.140
          1210
                    70.
                           0.198
                                                                3. 73
                                                                         33.5
                                                                                 31.0
                                                                                         0.140
Ţ
2
                           0.208
          1715
                                   *****
                                            *****
                                                     *****
                     75.
                                                                                         0.138
                                                                                 31.0
                                                                3.72
          1220
                     80.
                           0.217
                                   *****
                                            ****
                                                     *****
                                                                         33.7
                                                                                 31.0
                                                                                         0.138
          1226
                     86.
                           0.225
                                   ** ***
                                            *****
                                                     ****
                                                                3.71
                                                                         33.8
                                                                                 30.5
                                                                                         0.138
                                   ****
                                            *****
                                                     £275Æ
          1230
                    90.
                           0.227
                                                                3.71
                                                                         33.0
                                                                                 30.5
                                                                                         0.137
                                   *****
          1235
                    95.
                                            ****
                           0.234
                                                     *****
                                                                3.73
                                                                        33.9
                                                                                 30.5
                                                                                         0.138
          1240
                    100.
                           0.244
                                                     *****
                                                                3.74
                                                                         33.B
                                                                                 30.5
                                                                                         0.136
                                   *****
                                            *****
          1245
                    105.
                           0.254
                                                     * <del>* * * * *</del>
                                                                         33.9
                                                                3.66
                                                                                 33.5
                                                                                         0.136
                                   *****
          1250
                    110.
                           0.259
                                                                3.70
                                                                         33.9
                                                                                 30.0
                                                                                         0.137
                    115.
          1255
                           0.259
                                   *****
                                            ****
                                                     *****
                                                                3. 69
                                                                         33.9
                                                                                         0.136
                                   *****
                                            ****
          T300
                    170.
                           C.264
                                                     *****
                                                                3. 71
                                                                         34.1
                                                                                 30.0
                                                                                         0.132
 €
          1305
                   125.
                           0.263
                                    0.020
                                           . G.370
                                                     0.390
                                                                3.62
                                                                        34.1
                                                                                 29.5
                                                                                         0.134
          1310
                    130.
                           0.288
                                                     ****
                                                                3.68
                                                                         34.3
                                                                                 29.5
                                                                                         0.133
                                   *****
                                                                         34.2
                           0.298
                                                                3.69
                                                                                         0.133
                           0.303
 •
         1320
                   140.
                                   ****
                                                     ***
                                                                3.67
                                                                         34.3
                                                                                 29.5
                                                                                         0.131
          1325
                    145.
                           0.313
                                   ****
                                            *****
                                                     ****
                                                                3. 70
                                                                                         0.132
                                   ****
                                            ****
                                                                                 29.0
          T330
                   150.
                           0.310
                                                     *****
                                                                         35.3
                                   ****
 (
          1:335
                   155.
                           0.325
                                            ****
                                                     ****
                                                                3.67
                                                                        34.5
                                                                                 29.0
                                                                                         0.129
                                   ****
          1340
                                            *****
                   160.
                           0.332
                                                     ****
                                                                3.70
                                                                         35.6
                                                                                 29.0
                                                                                         0.129
                                   *****
          1345
                                            *****
                   155.
                           0.337
                                                                3.69
                                                                        35.6
                                                                                 29.3
                                                                                         0.129
         1350
                    170.
                           0.344
                                                                3.60
                                                                         35.6
                                                                                 23.5
                                                                                         0.129
                           0.352
                                                                3.65
                                                                         35.7
                                                                                 28.5
                                                                                         0.129
          1400
                   TEO.
                           0.357
                                   ****
                                            *****
                                                     *****
                                                                3.65
                                                                                         0.125
          1405
                   185.
                           0.362
                                    0.025
                                             C.310
                                                      0.335
                                                                3.67
                                                                         35.7
                                                                                 28.5
                                                                                         0.127
          1411
                   191.
                           0.371
                                            ****
                                                     * * * * * * * *
                                                                3.64
                                                                                 28.3
                                                                                         0.125
          1415
                   755.
                           0.376
                                                     * 4 * * * *
                                                                3.64
                                                                         35.7
                                                                                 24.5
                                                                                         0.125
                   200.
                                                     ***
 €
          1420
                           0.383
                                                                3.64
                                                                         35.7
                                                                                 23.0
                                                                                         0.123
          1425
                    205.
                           0.391
                                                     *****
                                                                3-61
                                                                         35.8
                                                                                 25.0
                                                                                         0.125
          1430
                    210.
                           0.396
                                                                3.53
                                                                                 25.)
                                                                         36.0
                                                                                         0.125
                                   ****
          1435
                   215.
                           0.431
                                                                3.62
                                                                         36.G
                                                                                 28.0
                                                                                         0-122
          1440
                                   ** * * * *
                                            *****
                                                     *****
                                                                3.62
                                   *****
          1445
                                           ****
                                                     ****
                                                                3.62
                                                                                         0.122
          1450
                                            ****
                   230.
                           0.423
                                   ****
                                                                3.53
                                                                         35.3
                                                                                 27.5
                                                                                         0-120
 1455
                   235.
                           0.425
                                   ** 4 7 * *
                                           ****
                                                     *****
                                                                3-6L
                                                                         35.0
                                                                                 27.5
                                                                                         C.121
          1500
                    240.
                           0.427
                                   ****
                                            ****
                                                     .....
                                                                         35.1
                                    `0.019<sup>--</sup>
          1505
                   245.
                           0.435
                                            0.261
                                                     0.280
                                                                3.55
                                                                        35.0
                                                                                 27.5
             ANNERS TAKET ---- DATA DISCAPOLO ? DUESTIDNABLE DATA
        DZONE COSAGE G1 0.10 = 41.80 PPM-MIN

DZONE COSAGE G1 0.08 = 46.32 PPM-MIN

NOZ-PAN COSAGE G1"6126 = 29.39 PPM-MIN
```

# 65-924   CCT-NTF-5098- 5-501   CF-8937 1970   BD 24-25	O-ASC.				,										1161	
#551, (9940)41314, 1105 65 400 25 600 25 600 600 600 600 600 600 600 600 600 60	12000 14240 14240 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340 14340	200 800 800 800 800 800 800 800 800 800	2,620 17.89 10.118 10.118 10.118 10.118	70 S S S S S S S S S S S S S S S S S S S	JE TC CALISA 1976 APE 15 ( 10%5) X16 198 045-NEA 3-WA) 04149 CHARGE 213-048 TC C	A CHE CALI AY VA CALI CALI		TO S4 1642- AMPLE JTENE	S4M9LE 2-CL0 E PORT							
raense en da de en esta esta en esta esta esta esta esta esta esta esta	and a second control of the control	1998 7 	भ्र ही	2-2-5071 VE 1415- 1915	1918, 1619;	10. I	ACPANALA NO VIOLENCE ACPANALA		0474		·					
CLPC (1945)	:	37	24.5		1545	1145	1245	1345	1445	1545	1645	1715	2015	2045 2045	2112	:
		60	CENTRAT	TOMS (P	(864)											
100 TO THE TOTAL THE TOTAL TO T	Janes .	1246	3200	31.70	3130	3140	3170	3090	3100	3110	2 4 4 4 5 4 5 4	* * * * * * * * * * * * * * * * * * * *	2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	* # * # * *	3040	٠
124 244 544	û bere	3 n	42.7 85.4	37.2	39.6	41.2	39.4	38.0	33.4	36.9	* * * * * * * *	* * *	* * *	***	35.4	·
	1 33	- 1	133	20 20 20 20 20 20 20 20 20 20 20 20 20 2	62.0	. 644.0 132	64.9	62.3	02.8 126	02.8 126	* * *	***	* * * * * * * *	* 1	121	
As a Stable	NI PPRC	64 %	46.2	39.2	42.3	45.1	42.3 35.6	42.1	41.0 62.0	47.8 95.5	* * * * *	* * *	* *	* #	36.5	
To the second	3866	5.5	13.9	14.3	13.9 41.6	14.1	14.2	14.5	14.3	14.1	15.5	15.2	5.85 28.5	5 5 5 5 5 5 5	29.5	
231 247 248 270 271 271	Post		0.11	11.4	10.9°	13.7	10.6	10.5	10.5	10.1	9.9	10.8 32.3	. 8. 4. 2. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	5.5	. 6.2 14.6	
1. 20° 2. 22° 24° 25° 25° 25° 25° 25° 25° 25° 25° 25° 25	Jrec	14 c)	25.	16.0 16.0	****	160	160 645	156 626	. 157	* *	160	159 635	91.7	91.5 305	43.7	
Construction	) Sad	25.5	8.08. 1.54	46.5	44.7	39.8	40.2 89.4	40.2	40.6	* #	41.8 83.7	85.3	23.4	23.6	63.5	
31.65 (6.245) \$2.50	2500	000 000	5.7	9 s	2.0	2.2	0.0	0.6	9.6	0.5	9.0	0.7 2.8	9.5	0.4 P.0		1
578-10 to 878-10		0.0	53.3	12.6	12.2	17.4	12.4	12.5	12.7	12.4	12.8	12.9	7.5	7.6 30.2	7.8	
243-318 THIL NOTHE	PSYBC	*****	46.7	43.9	46.3	46.1	112	45.7	45.6	44.3	46.4	46.1	26.6	101	42.7	:
2-863108 001685-2	2666	* * *	37.5	36.3	41.7	39.2	39.5	7.3 30.7	38.3	35.8	7.2	7.2 35.8	4.3	4.4	7.1	

		:			;
	2115	4*** 0.0.3	***** 27.9	175	14490.1 1203.3 1203.3
	2045 660	# # * * * *	* * *	721	\$ 5 5 7 C O
	2015	3 % * # # & * #	4 4 4 4 4 4	271	673.7
	215 545 1015 1045 1145 1245 1445 1545 1645 1715 2015 2045 2115 20 2045 2115 2045 2115 2045 2115 2045 2115 2045 2115 2045 2115 2045 2115 2045 2115 2045 2115 2045 2115 2045 2115 2045 2115 2045 2115 2045 2115 2115 2115 2115 2115 2115 2115 21	# # # # # #	25.5 32.1 33.0 31.6 31.9 4×44 30.4 28.5 0044 ×0044 0040	SOME 261 WANK 292 252 294 288 268 281 298 253 170 172 enve 291 291 293 253 170 172	1954.5 52.42.3 4840.3 4538.3 5124.3 5157.2 4785.0 5048.4 4603.6 **** **** **** **** **** **** **** *
	1645	* *	· · · · · · · · · · · · · · · · · · ·	298	**** 1170.3
	1545 360	60.6	28.5	281	6,000.6
	300	63.3	33.4	268	5048.4 1660.4 1650.4
٠.	1345	65.1	* * *	288	1785.0 1407.5
	1245	9.3	31.9	294	5157.2 1673.7 1673.7
	1145	6.53	31.6	252	5124.3
	. 1045	65.1	33.0	292	4538.3
	3015	63.5	32.1	# 4 # # # * # *	1720.3
	545	0 m	22.5	26.7	Million and and and and and and and and and an
	03 C	3.4	P TANK	## ## ## ## ## ##	en en en en en en en en en
CONTROL OF CONTROL OF A SECOND	SLOCK TIME SLAKIND TIME(MIN)	PPEC	57.2 - ( <u>M.</u> 97.5	The standard at the standard	

ACCTAGE DESTRUCTOR (ACCTAGE TO ACCTAGE TO AC		:			-	!			i	:	:					
GLOCK TING TI COSOL TICLITUDE		21.9	315		1416	1440	1015	1500	1115	1145	1215	1245	1315	1580	1415	
\$154.8x	:		C-96C-3TPAT (* 2960		· · · · · · · · · · · · · · · · · · ·	* * *	* * *	* * *	2960	* * *	* * *	3. 14 14 15 15 15 15 15 15 15 15 15 15 15 15 15	* * *	* * * * * * *	# # 6 6 7 <del>4</del> 4 6	-
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30745	0.107	8-61	15.0	15.9	16.1	16.0	15.9	15.9	15.7	15.5	15.2	15.1	14.9	39.3	14.4	
	5986	15.1	13.0	4.4	26.9	25.4	25.0	н. 3 25.0	5.5	10.0	± प्रक	9.5	3.7	2.3	0 + 0 0 + 0	
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ACCI (6.15)		25.04 feech	56.1	34.5	35.1	33.6	34.1	35.3	32.8	32.0	32.0	32.0	31.6	55.9	30.6	
3-2-607676	ပ အ စ	50	2.5	0.0 2.4	***	* *	***	2.2	0.4	0.0	0.0	0.0	0.0	0.0	0.0	
148127-4	3.3 35 32.5	45.4	11.4	45.5	44.0	10.5	5.01	10.7	7.8	0.0	0.0	0.0	0.0	37	9 Q 3 Q	
AND THE COURT BUILDING	2966	35.2	24.5	25.5	20.1	33.4	159	107	20.9	20.3	150	24.0	75.6	1119	123	
, 15 ·	Shad	00	5.56	5.2	5.0	5.2	5.3	5.4	9.4	0.0	0.0	0.0	00	0.0	0.0 0.0	
5. 6. 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	Saga	9 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	10.8	***	* *	* * * * * * * * * * * * * * * * * * * *	* * * * * * * * * * * * * * * * * * * *	\$ \$ \$ \$ \$ \$ \$	\$.4 55.5	* # * * * * * * * * * * * * * * * * * *	8.4 56.9	* * * * * * * * * * * * * * *	5 * 9 v	* * * * * * *	200	
21.3 1.87-7138	DEGG	***	27.9	****	***	***	* * * * * *	0 # 8 # 8 8 8 8	16.4	* *	11.5	> 7 8 % 8 %	55.1	***	41.6	
SICHLORS OTFUGREMETHANE	THANE PPRC	280	261	255	233	232	228	225	224	220	219	216	213	195 195	202	
DH BREALBHANN TRICL		1. 1.84C!	4621.8	******	890.7	* * * * & & & & & & & & & & & & & & & &	8484	876.0	4313.5	275.4	826.5	* : * is	3 0 5 5 7	5 € 5 € 5 € 5 € 5 € 5 € 5 € 5 € 5 € 5 €	**************************************	

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	1969		XX 化妆 化妆 化妆	· · · · · · · · · · · · · · · · · · ·	\$20X	新沙牛放 铁布布拉	13.5 40.5	0.0	79.4 313	57.9 55.6	0.0	0.0	15.5 92.8	0.0 0.0	大·安·安·安·安·安·安·安·安·安·安·安·安·安·安·安·安·安·安·安	· · · · · · · · · · · · · · · · · · ·	198 198	2688 505.9
	.1515 1830	783	245.0 2800	6.9	46.8	20.5 30.5	11.9	m	\$ 44. \$	26.7	0 0 0 0	သစ် စီစု	16.3	00	5.2	3.1	291	365.4 5
	1545 1900	(10115 (1923)	· · · · · · · · · · · · · · · · · · ·	公司 20 名 名 卷 卷 卷	最 人 等 之 表 。	*****	14.1	30	33.5	25.7	0.0	000	17.4	90	****	***	201	98 34 36
	1515	POENTER!	<b>经</b> 经	* * * * * *	*****	· 化二烷基	14.2	200 200 200	34.27	23.7	0.0	000	17.9	\$ 0.00 \$ 0.00	30.1	33.2	256	4444 5.23.3
:	1745	.00	等 整 等 等 者 类	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	· 51 · 4	5 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	14,1	20 mm	354	29.1	9.0	2.4.7	10.1	0.0	· · · · · · · · · · · · · · · · · · ·		208 208	57.7.5
1975 305 24-25 1976 305 24-25	(01k) swim 2 starps	•	36cc 314433x	DAME TO THE TOTAL STATE OF THE T	20 mg 2 mg	ACSEMICAS (POSODAS A)	)See	Since State of	Personal and the second	יישני נסאפי יישני	702.05-2-40.75°FF	0.13 to 1 to	2-3-01'strate bottle	2-38326 November 2	n nead a stantol	280d 113 17 KT 120		OB Skings - this Trib

SURROGATE RUN 223-U GLASS CHAMBER 1976 OCT 5

LIGHTS ON 1215, INTENSITY = 100% OF MAXIMUM
39 GC SAMPLES TAKEN; CO FACTOR 1.9/1.01; PAN CALIBR 9; BRADY 1296
1215 PAN SAMPLE WAS TAKEN AT 1221
AT T#0; TOTAL NON-METHANE HC# 2346 PPBC; METHANE= 2950 PPB

(	CLOCK	ELAPSED	OZONE	NO.	NO2-PAN	NOX-PAN	co	PAN	нсна	TS1	REL HUM
(	TIME 1	TIME (MIN)	(PP4) (	(Mea)	(PPM)	(PPM)	(PPM)	(PPH)	(PPM)	(DEG C)	
	1215	· · · · · · · · · · · · · · · · · · ·	0.0	0.150	0.143	0.287	5.63	0.001	0.040	 34•1	 61.0
	1230	15.	0.023	0.394	0.181	0.272	5.75	*****	****	33.1	63.0
	1245	30.	0.044	0.055	C.200	-0.251	5.75	0.006	***	33.8	63.0
	1300	45.	0.071	0.038	0.208	0.237	5.72	***	*****	33.6	62.5
	1315	60.	0.098	0.328	C.200	0.224	5.72	0.011	0.063	33.6	62.0
	1330	75.	* * * * * *	0.023	0.194	0.214	5.70	*****	*****	33.6	61.5
_	1345	90.	0.139	0.320	0.188	0.205	5.63	0.314	****	33.7	61.0
€ .	1400	105.	0.159	0.317	0.181	0.194	5.61	****	****	33.8	60.5
	1415	120.	C.181	0.015	9.173	0.185	5.57	0.018	0.095	34.0	59.5
_	1430	135.	0.203	0.024	0.157	0.176	5.56	****	****	34.1	59.0
(	1445	150.	0.222	0.312	0.161	0.165	5.52	0.021	****	34.0	58.5
	1500	165.	0.242	0.311	0.153	0.160	5.51	*****	****	34.2	58.5
_	1515	180.	0.259	0.310	0.147	0.154	5.53	0.022	0.081	34.3	57.5
C	1530	195.	0.275	0.010	0.140	0.145	5.46	****	****	34-5	57.5
	1545	210.	0.298	0.010	0.132	0.139	5.48	0.025	*****	34.5	57.0
	1600	225.	0.318	0.007	0.125	0.130	5.43	****	*****	34.6	56.5
C	1615	240.	0.337	0.012	0.124	0.131	5.39	0.027	0.024	34.7	55.0
	1630	255.	0.354	0.337	0.114	0.116	5.43	***	*****	34.8	56.0
	1645	270.	0.374	0.306	0.105	0.109	5.42	0.031	***	34.9	55.5
C	1700	285.	0.393	0.305	0.099	0.101	5.38	****	*****	34.9	55.5
C	1715	300.	0.410	0.005	C.393	0.095	5.42	****	0.051	34.8	55.0
	1730	315.	0.427	0.005	0.038	0.389	5.38	*****	****	34.9	55.0
C.	1745	330.	0.445	0.005	0.061	0.981	5.35	****	***	****	55.0
	1800	345.	0.462	0.007	C-074	0.075	5.39	****	****	*****	54.5
С.	1815	360.	0.479	0.002	0.068	0.069	5.37	0.039	****	34.7	55.0
٠.	***	*** NO (	DATA TAKÉN		DATA	DISCARDE	D D	?_QUEST[	GNABLE C	AIA	,
C.	OZONE	DOSAGE	GT 0.13 =	53.58	PPM-MIN					•	
	DZONE	DOSAGE	GT 9.09 =	64.66	PPM-MIN						
Č	NO2-PAN	BD24GE	GT 0.25 =		PPH-MIN	111		** * ***	Marie and about the light broad may be	**** * **	<del></del>
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1345-595 SAMPLE USEC ON PORPORA N 4CETALDEHYDE, PROPICNALCEHYDE, ACETONE, BUTYRALDEH TOLUENE AND M-KYLENE FROM 3P	FC ON PC	F ON POL	V CETONE,	BUTYRAL	UTYRALDEHYDE	AND ME	AND MEK_FROM C-600	2-600				,	***************************************	: 4		:
GLOCK TIME ELLYSED TIME(MIN)		1015	1132	1215	1230	1245	1300	1315	1330	1345	1400 105	1415	1433	1440	165	
		CO	CONCENTRATIO	: Z	S (PPB)						-	1			:	•
HETHANG	PPBC	1120	* * * * * * *	2950	* * * * * * * * * * * * * * * * * * * *	**	* * *	2920	* * *	***	* *	.2880	* * *	* * * * * * * * * * * * * * * * * * *	* 3 5 5 5	
THE THE PARTY OF T	PPSC	1.3	* *	* * *	4 4 4 4 4 4	* *	* * * * * * * * *	* *	* * *	30.1.	* *	51.5	* * * * * * * * * * * * * * * * * * *	* * *	* * * * * * * *	
ETHAME COLORS	PPBC	4.2	* * * * * * * *	* * *	* * * *	* * *	* * *	* * *	* * *	84.9	* * * * * * *	81.0	\$ <b>*</b>	* * *	# 3 # # # 3	
ACETYLENE (POPOPAK	A) PPBC	2.4	* *	* * *	* *	* *	* * *	* * *	* *	42.3	* *	38.6	* * * * *	5 5 4 4 5 5 2 4	* * * *	
разране	PPBC	12.9	* *	20.0	* *	19.6	* * *	18.9	* # * * * #	* * * * * * * * * * * * * * * * * * *	* *	13.3	* * * * * * * * * * * * * * * * * * *	* * *	10.2	
BNB dC dd	PPBC	2.1	12.9	12.9	* * *	8.7	* *	19.5	* * * * *	本 本 4 本 4 本	* *	12.0	3 # 3 # 8 3 8 4	***	2.t.	:
SOBUTANE	PPAC	0.1	* * *	**	***	* * *	***	* * *	* * *	***	# # # # # #	* * *	* * *	* *	* * * * *	
N-BUTZNE	PPBC	3.5	198	196	* *	186	* *	4 4 4 4 4 4 4 4	* *	* *	# # # * # #	171	3 9 4 4 5 4 5 4	4 # 4 # 4 #	164	
ACETYLENE (DES)	PPBC	5.5	42.4	42.5	* *	42.5	* *	42.5	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	***	***	41.4	***	***	19.2	
TPANS-2-BUTENE	ррис	0.0	3.2	3.2	* *	1.2	* *	0.0	* * *	* *	* *	0.0	* *	* 4 * 4 * 5	0.0	
I SOPENTANE	PPBC	1.5	3.5	4.5	* *	5.0	* * *	5.5	* * *	* * *	# # # # # #	5.5	* * *	5 5 5 5 7 8	1.2	
CIS-2-BUTENE	PPBC	0.0	14.8	58.4	* *	5.2	* *	1.7	* *	* *	* *	0.0	* *	* * * * * * * * * * * * * * * * * * *	0.0	
N-PEDTANE	PPBC	0.0	1.0	1.5	* *	1.5	* * *	2.5	* *	* *	* * *	2.5	**	* * *	**	
2,3-01METHYL BUTANE	PPBC	0.0	109	110	* * *	59.5	* *	93.1	* * * * * *	4 4 4 4 4 4	# # # # # #	84.6	4 4 4 4 4 4 4 4	# # # # # #	19.5	1

SLAROGATE 223-U GLASS CHAMBER 1976 OCT 5	i											8 8 8 8 8			1977 MAR 18	:
CLOCK TIME ELAPSED TIME(NIN) -120 -43	1	1015	1132	1215	230 15	1245	1300	J315 60	1330 1345	1345	1400	120	1430	1445	1500.	
PP6C 0.0 81.0	PPEC	0.0	81.0	83.0	***	12.0	<b>操</b>	0.0	春春	<b>松</b>	*	0.0	*	*************************************	0.0	1
ACETALCEHYDE	PPBC	- 1	2.8 **** 5.6 ****	* * * * * * * * * * * * * * * * * * *	* * * * * * * * * * * * * * * * * * * *	* *	* *	* * *	# # # # # # # #	* * *	* * * * * * * * * * * * * * * * * * *	* *	* * *	* * * * * * * * * * * * * * * * * * *	***	-
PROPICHALCEHYOF	PPBC	0.2	* 4 * 4 * 4 * 4 * 4 * 4 * 4 * 4 * 4 * 4	E 0	* *	* *	本 本 本 本 本 本	* * *	* * * * * * * * * * * * * * * * * * *	* * *	· 本 本 · 本 本 · 本 本	2.6	* 4 * 4 * 4	* * *	· · · · · · · · · · · · · · · · · · ·	
ACETCNE	реяс	7.0	1	7.9	* *	<b>安安</b> 安安 安安	* * * *	# # # # # #	* * *	* *	* * * * * * *	36.6	\$ 5 \$ 5 \$ 4 \$ 4	# # # # # #	<b>等性的</b> 等	1
METHYL ETHYL KETONE	рРВС	Dre PPBC 1.2	* *	1.8	* *	* *	* * *	* *	> 4 4 4 3 9 4 4	* *	* * *	32.8	# # # # # #	* * * * * * * * * * * * * * * * * * *	**************************************	
TCLUENE	рряс	0.2	15.5	16.1	# 4 4 4 4 4 4 4	14.4	* *	13.5	5 4 5 4 4 4 4 4	* *	# 4 # 4 # 4	12.6	* * * * * * *	* *	* * * * * * * * * * * * * * * * * * * *	
META-KYLENE	2866	0.0	52.3	53.1	* * * * * * * * * * * * * * * * * * * *	37.1	3 4 4 4 3 3 4 4	29.9	* * * * * * * * * * * * *	* * * * * * * * * * * * * * * * * * *	* *	22.3 178	* * * * * * * *	* * *	**	
BUTYRALCEHYDE	PPBC	1.0	* *	0.1	* *	* * *	* *	* *	* * * * * *	* *	·	1.0	5 4 7 4 7 4 8 5	* * * * * * * * * * * * * * * * * * *	**************************************	1
DICHLOKO DIPLUDROMETHANE	PPBC	0.0	355	351 351	* * *	347	* *	0.00 0.00 0.00 0.00	* *	* * *	* * 4 & 4 &	337	* * * * * * * * * * * * * * * * * * *	* # *	327	i
TOTAL HC PPBC TOTAL NON-METHANE HC TOTAL SURROGATE		1178.3 **** 58.3 2241.5 46.5 2237.0		5647.3 2345.9 2307.7	* 0 * *	**** **** 0.0 1949.5 **** 1943.0	7 **** ****	**** 4326.8 0.0 1068.1 **** 1060.1	***	315.8 315.8	**** 5204.3 0.0 1987.2 **** 1824.8	204.3 987.2 824.8	0 · 0 · · · · · · · · · · · · · · · · ·	7 0 0 0 ± 0 ± 0 ± 0	#### 1.1283.2 # 1.274.2	:
			***************************************		-											†

ETHANE. POBC	1515	1530	210	1600	1615	1630 255	1645	285	300		
METHANE, POB		CONCENTRA	ATTONS (P	1844	.						
	2900 C 2900	***	* *	* * *	2810	* *	* * * * * * * * * * * * * * * * * * * *	* *	2880 2880		
3446 3446	23.7 C 47.4	* * * * * * * * * * * * * * * * * * * *	* * * * * * * * * * * * * * * * * * * *	* * * * * * * * * * * * * * * * * * *	20.3	* *	* * *	* * * * * * * * * * * * * * * * * * * *	16.1		
ETHANE	78.6 C 157	· ·	* *	を 4 を 4 を 4 か 6	78.0	* *	# ** # # # #	4 4 4 4 4 4 4 4 4 4	74.9		
ACETYLENE (PGP3PAR N) PPBC	35.d C 71.6	* * *	* * *	# % * * * *	35.7	* * *	* * *	* * * * * * * * * * * * * * * * * * * *	36.8 73.6		
D804 9980	* * * *	18.4	* * *	18.0	* *	18.0	* *	* *	17.6 52.8		
PROPERE	* * *		* * *	1.4	* * * * * * * * * * * * * * * * * * * *	0.9	* *	* * *	0.6 1.8		
I STRUTANE PORC	4 4 4 4 4 4 4 4 4 4	* *	* *	* * * * * *	* * *	* * *	4 4 4 4 4 4	* *	· · · · · · · · · · · · · · · · · · ·		;
N-30Tans PPBC		162	李 杂 桂 春 春 春	156 626	* * * * * * *	451 451	* * *	* * *	144 574	. :	
ACETYLENE (DWS) PPBC	* *	40.3	* * *	39.5	* * * * * * * * * * * * * * * * * * * *	38.8	# # # # # #	# # # # # #	37+3 74-6		; ; ;
TRANS-2-BUTENF PPBC	***	0.0	* *	0.0	2 4 2 4 3 4 4 4	. 00	* *	* * *	0.0		! ! !
ISOPENTANE	* * *	1.3	* * *	1.3	# X # # # #	3.0	* *	* *	S • 1		· ·
C15-2-auteur PPBC	* *	0.0	* *	000	* * *	0.0	0 # 0 % 4 #	* * * * * *	0.0		
N-PENTANE PPBC	* *	2.5	* *	900	* *	0.5	* * *	# # # # # #	7.0		:
Z.)-DIMETHYL BUTANE PPBC	4 # 4 # 4 #	76.6	> 0 > 0 0 4 0 4	72.2	* * * * * * * * * * * * * * * * * * * *	69.7	# # # # # #	# # # # # # # #	63.5		
Z-WETHYL BUTENE-2	0.0	16.2 81.0	16.6	4 4 4 4 4 4 7 7	2.4	* *	0.0	* * * * * * * *	# # # # \$ # \$		
ACETALCEHYDE PPBC	* *	* *	* *	* * * * * * * *	* * * * * * * * * * * * * * * * * * * *	# # # # # #	# # # # # #	* *	***		
PROPICNAL CEHYDE	* *	****	* * *	* *	4.0	* * * * * * * * *	* *	* *	4.8 14.4		

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# APPENDIX C

Plots of  $\ln$  SO $_2$  vs. time for AGC Runs 216 through 222

